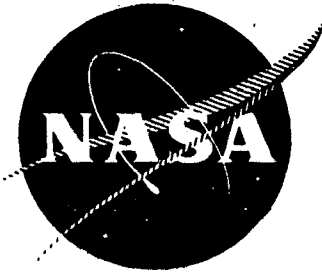


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ACOUSTIC TESTING OF A 1.5 PRESSURE RATIO,  
LOW TIP SPEED FAN (QEP FAN B SCALE MODEL)

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by

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GENERAL ELECTRIC COMPANY



prepared for

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NASA-Lewis Research Center  
Contract NAS 3-12430  
James J. Kramer, Project Manager

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I. ABSTRACT

A scale model (.484 scale factor) of a single stage fan designed for a 1.5 pressure ratio and 1160 ft/sec (353.6 m/sec) tip speed was tested to determine its noise characteristics. The fan had 26 blades and 60 outlet guide vanes, with vanes spaced two rotor blade aerodynamic chords from the blades. The effects of speed, exhaust nozzle area and fan frame acoustic treatment on the scale model's noise characteristics were investigated.

Level flyover projections to a full scale engine of 22,000 pounds (97,900 newtons) static thrust indicates single fan noise levels of 98.6 PNdB at approach [370 ft (112.8 m) altitude, flight Mach number 0.25, 4900 pounds (21,805 newtons) net thrust] and 98.4 PNdB at takeoff [1000 ft (304.8 m) altitude, flight Mach number 0.25, 16,000 pounds (71,200 newtons) net thrust] for the untreated fan with nominal nozzle. The corresponding configuration with acoustic treatment in the fan frame resulted in 94.3 PNdB at approach and 94.6 PNdB at takeoff. The noise reductions occurred at the blade passing frequency and harmonic tones as well as in the broadband noise.

Runs with exhaust nozzles 16% oversized and 6% undersized showed similar results.

## II. SUMMARY

A scale model fan, designated "Fan B," was utilized to determine the acoustic characteristics of a single stage fan designed for a corrected tip speed of 1160 ft/sec (353.6 m/sec) at a bypass pressure ratio of 1.5. The fan had 26 rotor blades and 60 vanes with 2 rotor aerodynamic chord spacing between the rotor and the OGV's. The scale model fan which represented a .484 linear scale model version of the full scale Fan B, simulated the bypass flow region through the fan.

The scale model was tested to determine the effects of speed, exhaust nozzle area and fan frame acoustic treatment on the fan's noise characteristics. Acoustic data was recorded at ten speed points covering a range from 30% to 100% sea level static thrust. The fan was tested with three different nozzles - nominal, 16% oversize and 6% undersize - for this sequence of speed points in order to identify operating points which would produce lower noise at a given thrust level. Each set of tests was run with and without acoustic treatment in the fan frame. This frame treatment consisted of 1/2 inch (1.25 cm) thick Scottfelt covered with a 22 1/2% porosity plate.

The data obtained at each of these test points was scaled up to full scale to evaluate the projected effectiveness of the design in reducing the noise of the fan system. Projections of a full scale, uninstalled, 22,000 pounds (97,900 newton) static thrust engine with nominal nozzle indicate the following single fan, maximum Perceived Noise Levels (PNL) for a level flyover:

FAN B LEVEL FLYOVER PROJECTIONS  
MAXIMUM PERCEIVED NOISE LEVELS  
SINGLE FAN

	<u>Untreated</u>	<u>Treated</u>
Takeoff 1000 ft (304.8 m) altitude $M_o = .25$	98.4 PNdB	94.6 PNdB
Approach 370 ft (112.8 m) altitude $M_o = .25$	98.6 PNdB	94.3 PNdB

The 200 foot (61.0 m) sideline, maximum PNL's for all three fan exhaust nozzles, treated and untreated, at approach and takeoff thrust are summarized below for a single full scale Fan B.

Full Scale Fan B  
200 Foot (61.0 M) Sideline, Maximum PNL

	Approach*	Takeoff**
Nominal nozzle, untreated	104.4 PNdB	116.6 PNdB
Nominal nozzle, treated	100.2 PNdB	112.4 PNdB
Large nozzle, untreated	106.0 PNdB	117.2 PNdB
Large nozzle, treated	100.8 PNdB	113.6 PNdB
Small nozzle, untreated	106.8 PNdB	117.5 PNdB
Small nozzle, treated	101.6 PNdB	113.6 PNdB

\* 6,684 pounds (29,744 newtons) static fan thrust

\*\*17,140 pounds (76,277 newtons) static fan thrust

The nozzle size variations did not produce any appreciable new low noise operating points for approach or takeoff rated fan thrust. However, thru the mid-thrust region, the large nozzle resulted in the lowest sideline PNL in both the treated and untreated configurations.

### III. INTRODUCTION

This report describes work performed by the General Electric Company for the NASA-Lewis Research Center on the Experimental Quiet Engine Program.

The major objectives of this program were:

- (1) To determine the noise levels produced by turbofan bypass engines designed for low noise output and to confirm that predicted noise reductions can be achieved;
- (2) To demonstrate the technology and innovations which will reduce the production and radiation of noise in turbofan engines;
- (3) To acquire experimental acoustic and aerodynamic data for high bypass turbofan engines from which acoustic theory and experience can be correlated to provide a better understanding of the noise production mechanisms.

A scale model fan program was utilized to provide information pertinent to achieving these objectives. The results of the scale model testing provided directly applicable experimental data on noise reduction features that might be applied to full size fan systems. Experience indicates that such scale model acoustic tests provide accurate and effective means to readily evaluate such low noise design configurations.

Fan B was incorporated into the NASA/GE Quiet Engine Program to investigate the noise generating and radiating characteristics of a low speed, moderately loaded, single stage fan. The Fan B scale model, the first scaled fan tested, was approximately a half scale version (48.4%) of the full size fan and it essentially reproduced the bypass flow region through Fan B.



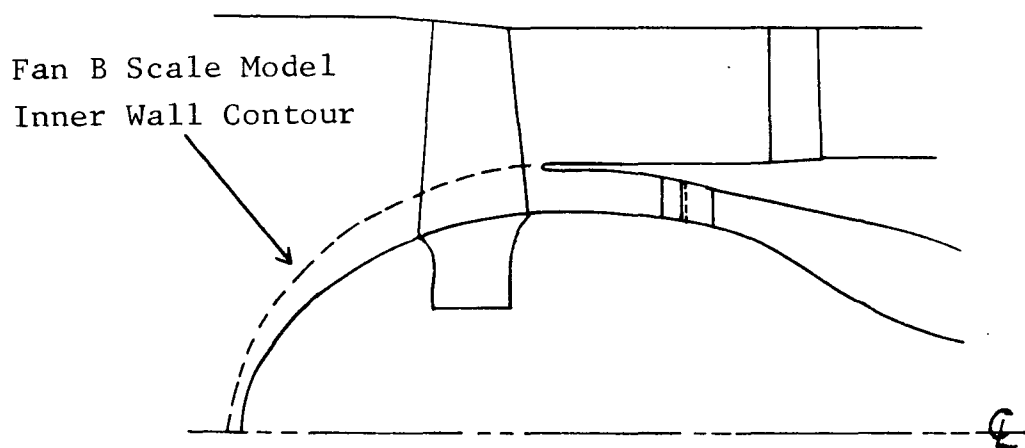
The effects on the scale model's noise characteristics of speed, exhaust nozzle area and fan frame acoustic treatment were examined during the first phase of testing. Acoustic data was recorded at speed points corresponding to a range from 30% to 100% sea level static thrust. The fan was tested with three different nozzles for this sequence of speed points in order to identify operating points which would produce lower noise at a given thrust level. Further, each set of tests was run for two configurations, designated untreated and treated, to determine the effectiveness of the fan frame acoustic treatment. The data obtained at each test point was scaled up to full scale to evaluate the projected effectiveness of each design in reducing the noise of the fan system.

#### IV. Test Vehicle Description

Full scale Fan B is a low speed, moderately loaded, single stage fan. It has been designed at the altitude cruise condition for a corrected tip speed of 1160 ft/sec (353.6 m/sec), at a bypass pressure ratio of 1.5 and with a corrected fan flow of 950 lb/sec (430.9 kg/sec). This fan incorporates 26 shroudless rotor blades and 60 outlet guide vane (OGV's) with a rotor - OGV spacing of two aerodynamic rotor chords to minimize noise generation.

The scale model used to determine the acoustic characteristics of different low noise designs, essentially simulated the bypass portion (outer 84.5% of flow) of the full size Fan B, as shown schematically in Figure 1. The design basis was to provide the same corrected tip speed, pressure ratio and weight flow per unit area as the bypass portion of the full scale Fan B. To maintain the bypass pressure ratio on the scale model, it was necessary to increase the loading at the hub to account for the end-wall-blade boundary layer interaction. Figures 2 and 3 show the scale model Fan B aerodynamic characteristics - pressure ratio vs corrected weight flow and corrected weight flow vs percent corrected fan speed, respectively - for three nozzle sizes. Some other pertinent scale model and full scale characteristics are shown in Table II.

The effects of varying the fan operating line were investigated with the scale model by running three nozzle sizes, consisting of 372 sq. in. ( $.24 \text{ m}^2$ ), 396 sq. in. ( $.26 \text{ m}^2$ ), and 460 sq. in. ( $.30 \text{ m}^2$ ), or about 6% less than nominal, nominal and 16% greater than nominal, with the nominal nozzle being equivalent to a  $1700 \text{ in}^2$  ( $1.10 \text{ m}^2$ ) nozzle on the full scale fan. The nozzle variations were run on both treated and untreated configurations.



Schematic of Fan B

Figure 1

# QUIET ENGINE PERFORMANCE SCALE MODEL FAN B

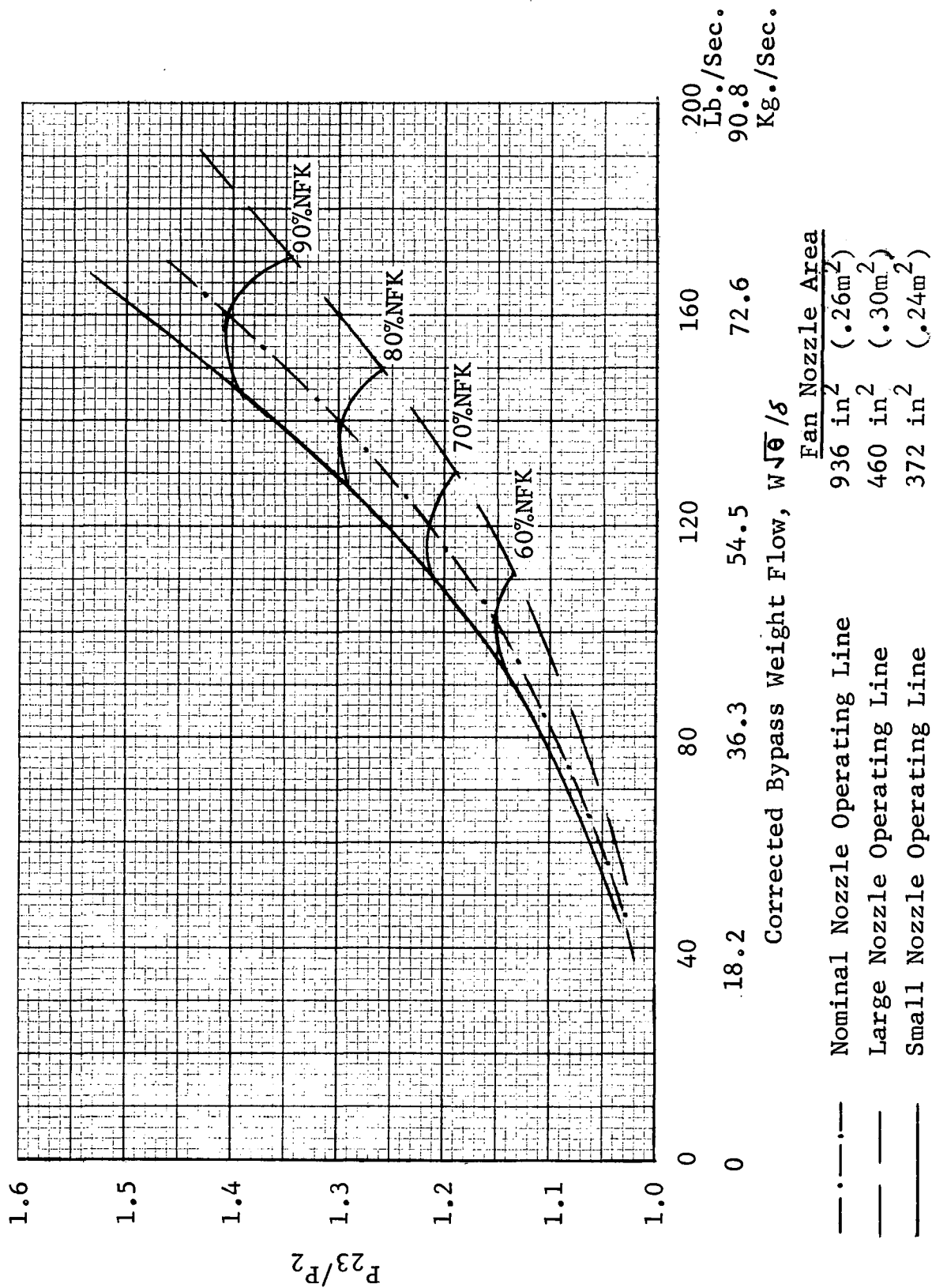


Figure 2

QUIET ENGINE PERFORMANCE  
SCALE MODEL FAN B

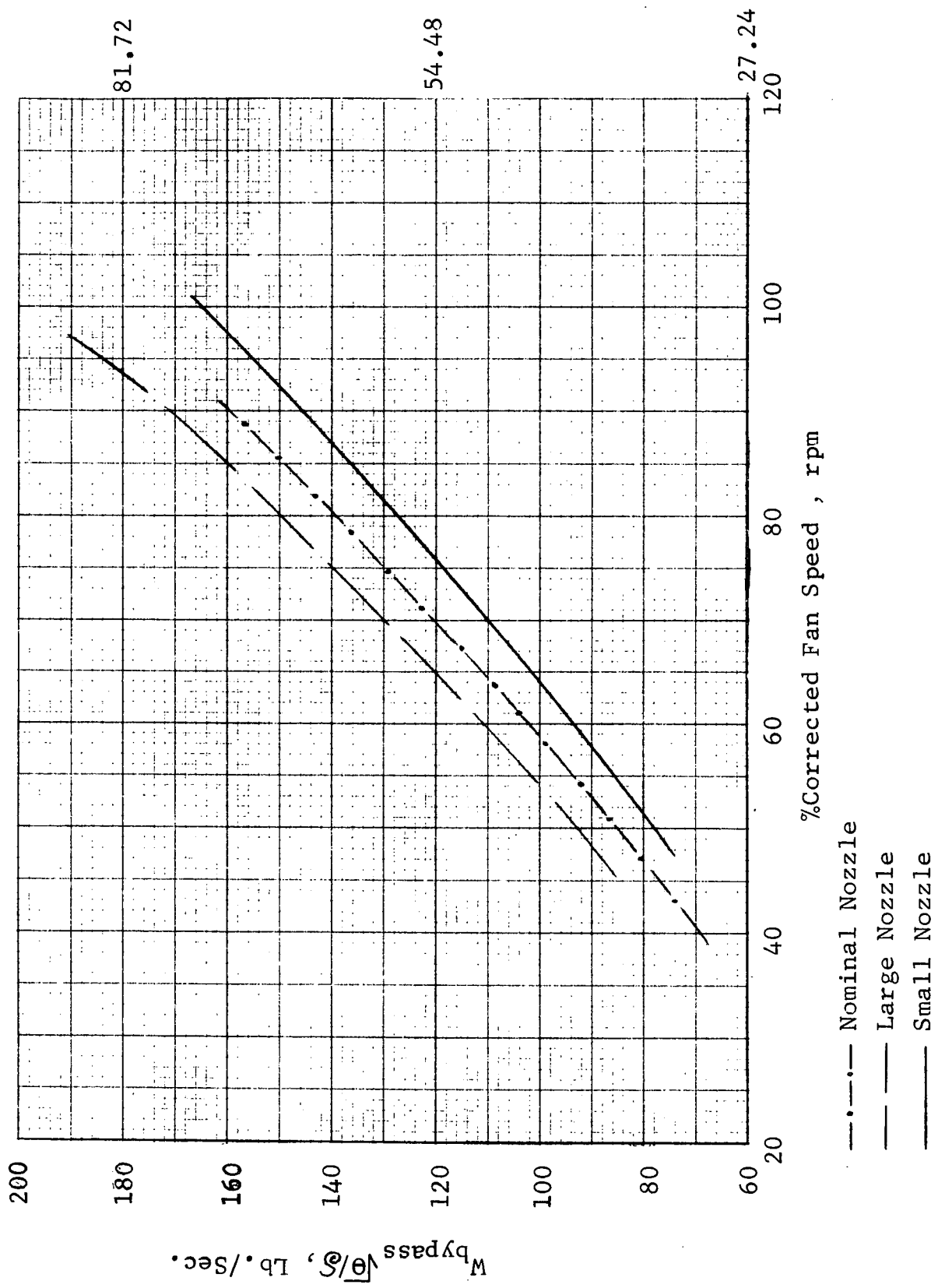


Figure 3

TABLE I  
QEP FAN B  
FULL SCALE AND SCALE MODEL CHARACTERISTICS  
SEA LEVEL STATIC, STD. DAY  
TAKEOFF POWER - 91% FAN SPEED

	<u>Full Scale</u>	<u>Scale Model</u>
100% Speed, RPM	3625	7488
Tip Speed, Ft/Sec (M/Sec)	1055 (322)	1055 (322)
Bypass Total Pressure Ratio	1.415	1.415
Bypass Flow, Lb/Sec (Kg/Sec)	692 (313.9)	162 (73.5)
Fan Duct Thrust, Lbs (Newtons)	17,140 (76,277)	4010 (17,844)
Rotor Inlet Tip Diameter, Inches (M)	73.35 (1.9)	35.5 (.9)
Inlet Hub/Tip Ratio	.465	.579
Number of Rotor Blades	26	26
Number of OGV's	60	60

The acoustic treatment of the fan frame area was scaled from the full scale fan and incorporated in the scale model. Figure 4 shows a cross section of the fan indicating the location of the acoustic treatment. The amount of acoustic treatment at each location is listed in Table III. The areas shown are effective areas, allowing for fasteners, assembly methods, rake pads, support ribs, etc. The treatment material used on the scaled fan was Scottfelt 3-900,  $\frac{1}{2}$ " (1.3 cm) an open-celled polyurethane foam material, having suppression characteristics similar to the Multiple-Degree-of-Freedom resonator suppression material used on the full scale vehicle. The scale model treatment was held in position by means of a perforated face plate with 1/16 inch diameter holes and a porosity of 22 1/2%.

For the untreated configurations, the treatment was neutralized by covering with an adhesive backed foil tape.

FAN B SCALE MODEL  
CROSS SECTION INDICATING LOCATION OF ACOUSTIC TREATMENT

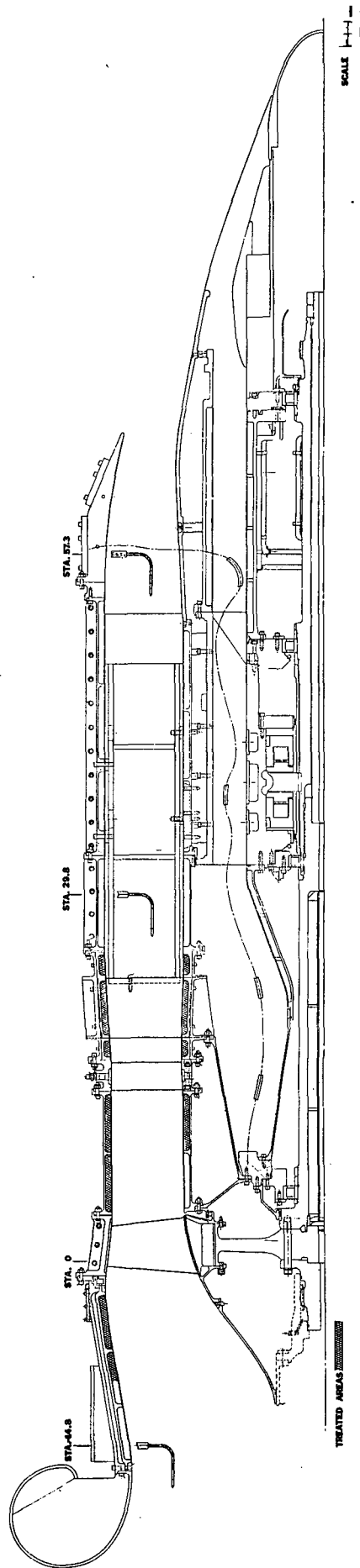


Figure 4



TABLE II  
QEP SCALE MODEL FAN B  
ACOUSTIC TREATMENT AREAS

<u>LOCATION</u>	<u>AREA</u>	
Inlet	812 in <sup>2</sup>	5240 cm <sup>2</sup>
Rotor - OGV's		
Inner Wall	315 in <sup>2</sup>	2030 cm <sup>2</sup>
Outer Wall	1007 in <sup>2</sup>	6500 cm <sup>2</sup>
Aft of OGV's		
Inner Wall	417 in <sup>2</sup>	2690 cm <sup>2</sup>
Outer Wall	668 in <sup>2</sup>	4310 cm <sup>2</sup>
Total	3219 in <sup>2</sup>	20,770 cm <sup>2</sup>
	22.4 ft <sup>2</sup>	2.08 m <sup>2</sup>

## V. Test Program

Testing of the scale model vehicle was performed at the Peebles Test Operation, General Electric's out-door test facility shown in Figures 5 and 6. Testing was performed on Site 4B, using a G.E. LM1500 stationary gas turbine as the drive system. Figure 7 shows a typical scale model vehicle installation. As can be seen, the scale model fans were driven from the front to eliminate noise generation by discharge flow over the drive structures.

### A. Farfield Data Acquisition

The acoustic data was taken with microphones located on a 100 foot (30.5 m) arc, positioned at 10 degree increments from 20° to 160° as measured from the fan inlet centerline at the rotor leading edge. The microphones were set at the height of the fan centerline, 12 feet (3.7 m) above the sound field surface. This sound field surface consisted of a level, 250 ft. (76.2 m) arc of crushed stone.

Data was recorded on FM with a Sangamo 28 channel recorder, Model 4700. A tape speed of 60 ips (1.5 m/sec) was used to provide a flat frequency response through the 20 KHz 1/3 octave band. Data was recorded for a minimum of 60 seconds, with all angles being recorded simultaneously.

Each microphone system consisted of the following equipment:

<u>Component</u>	<u>Manufacturer</u>	<u>Model</u>
Microphone	B & K	4133 ½ inch (1.3 cm)
Cathode Follower	B & K	2615
Power supply	B & K	2801

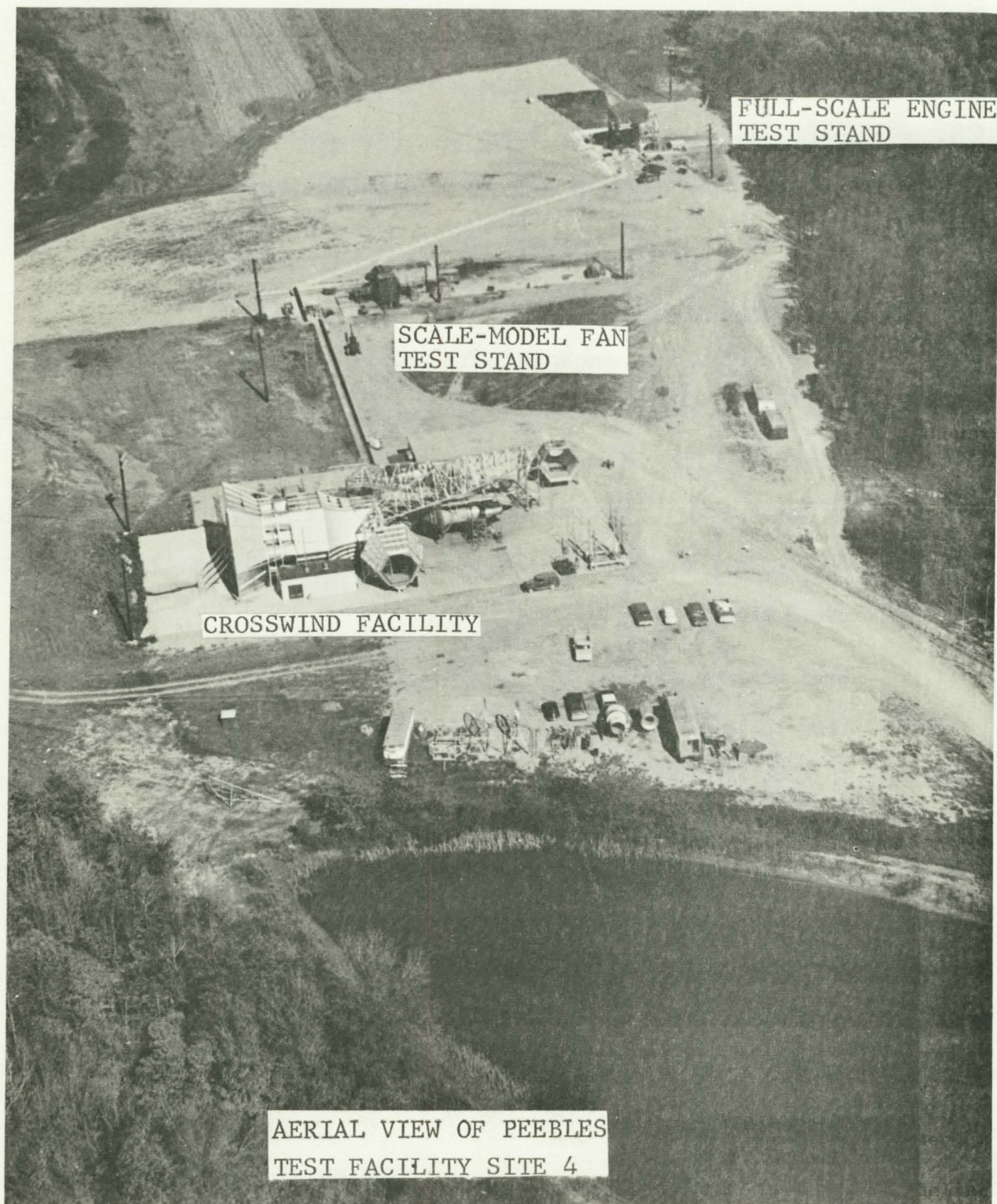


FIGURE 5



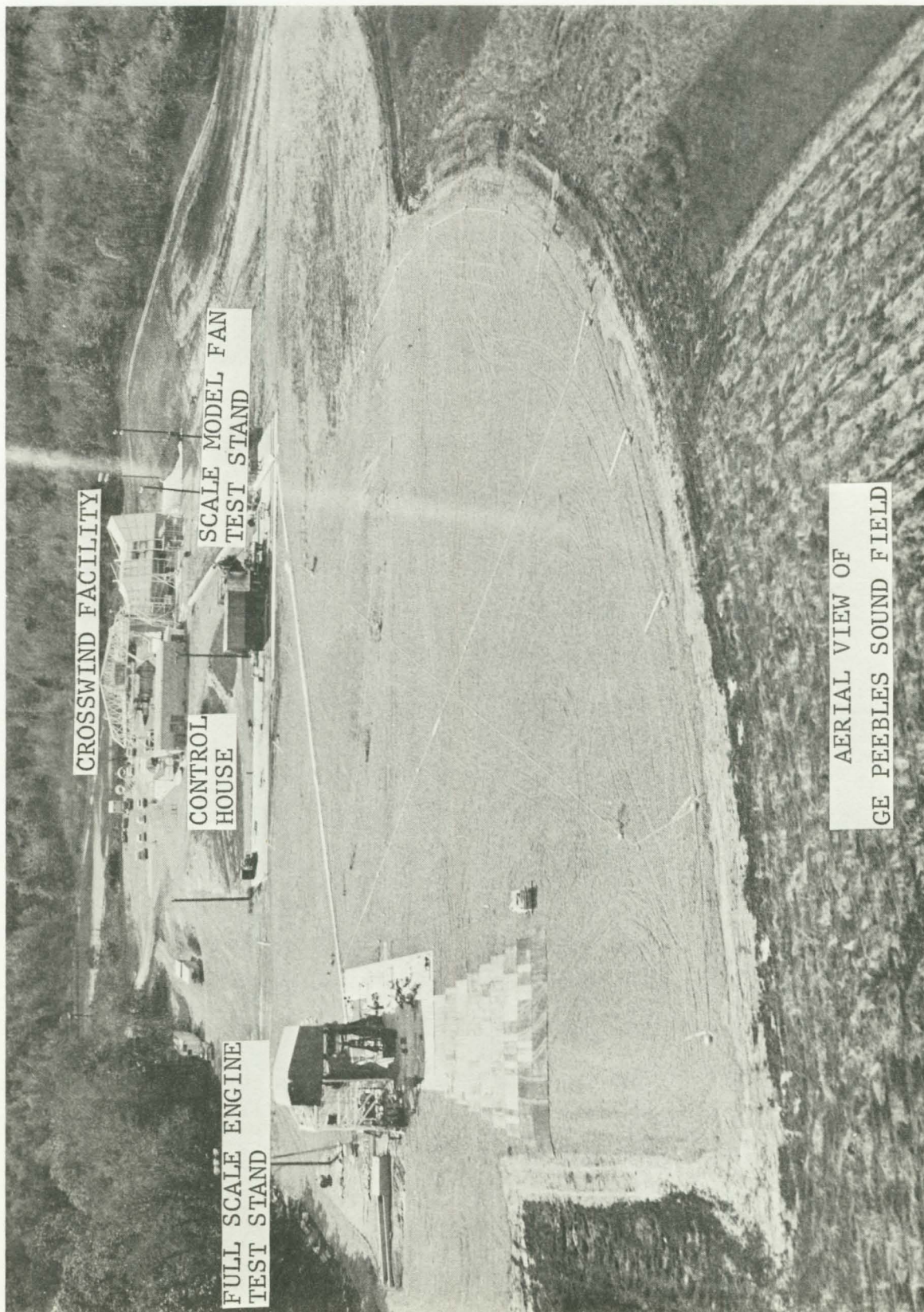
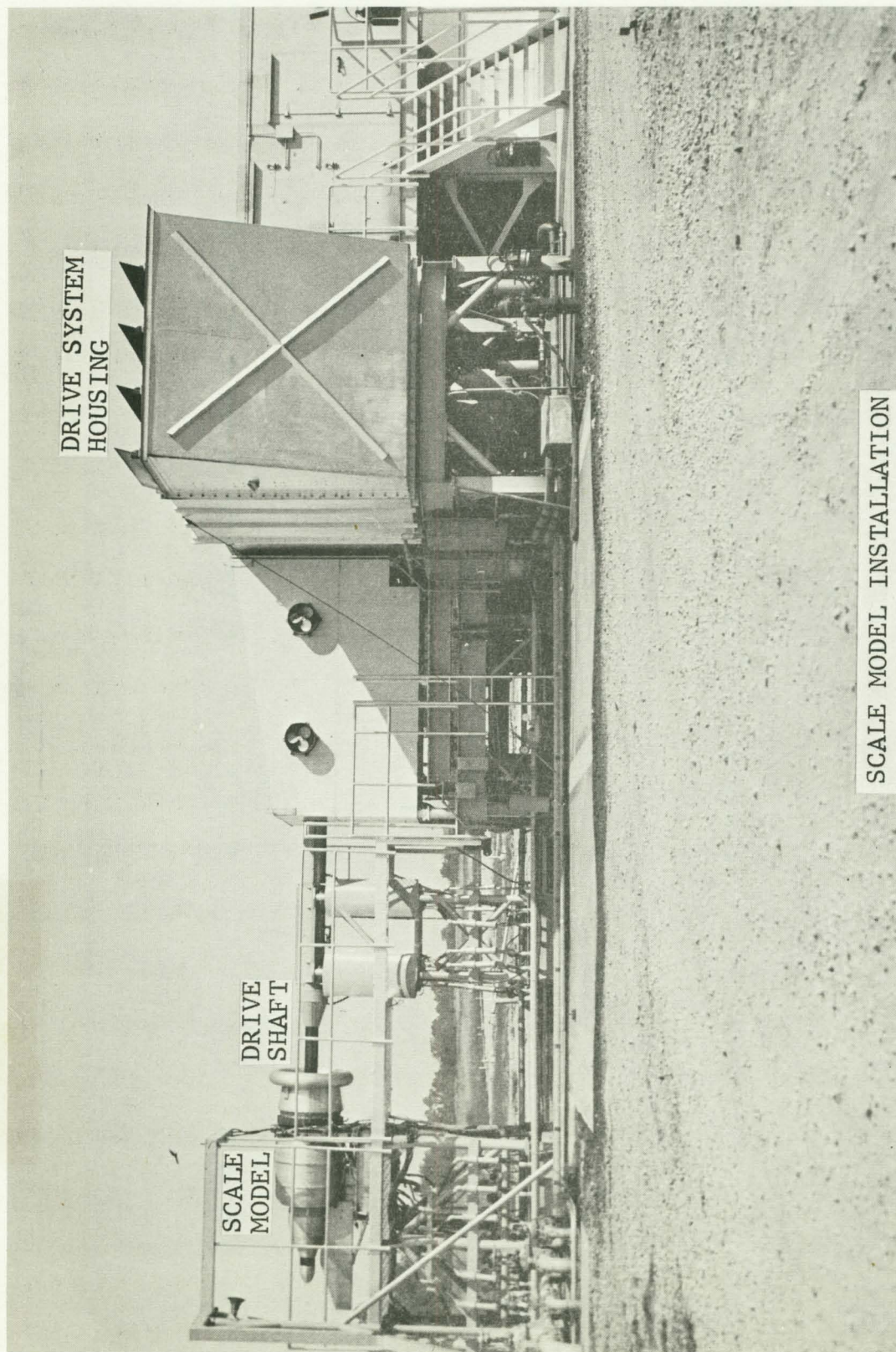


Figure 6

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SCALE MODEL INSTALLATION

Prior to testing, the frequency response of the system was determined by removing the microphone head and inputting a constant voltage at various frequencies throughout the range of interest. For a range of 50 Hz to 25 KHz, this was performed at frequencies of 50, 250, 1000, 5K, 8K, 10K, 12.5K, 16K, 20K and 25KHz. The voltage input was chosen at 10 millivolts, approximately the equivalent to 94 dB for a ½ inch (1.3 cm) microphone and an approximation of the levels encountered during an actual test.

The loss through each system was measured by removing the microphone head and inputting one volt RMS at the microphone preamplifier at a frequency of 250 Hz, to correspond with the pistonphone frequency. If the system loss was not within a specified limit, based on the specifications of the components, then the system was checked and/or changed before continuing.

With the 124 dB pistonphone on the microphone, the voltage output was compared with the calculated output based on the system losses and the microphone sensitivity. If the actual voltage output agreed within ½ dB (approximately 5%) of the calculated output, the microphone was functioning properly. Microphone cartridges falling outside this limit were set aside for repair and/or recalibration prior to reuse.

The amplifiers, tape recorder, and data reduction facilities were checked by recording a broadband electrical signal of known amplitude, known as "pink noise." Reduction of this signal provided a measure of the frequency response of these components.

In addition to these system checks, a pre and post test calibration was recorded on each channel using the 124 dB pistonphone (B&K model 4220).

## B. Testing Schedule

Acoustic tests were conducted at ten speed points, with three nozzle sizes, for both the untreated and treated configurations. Table IV summarizes the configurations for which data was obtained.

The speeds selected correspond to the net engine thrusts shown below:

RPM	% SPEED	% F <sub>n</sub> SLS <sup>*</sup>	% F <sub>n</sub> alt=0 <sup>**</sup> M = .25
4040	54.0	29.5	22.3
4474	59.8	36.8	30.6
4700	62.8	40.9	35
4907	65.5	45.2	40
5505	73.5	58.6	55
5990	80	71.1	70
6354	84.9	81.9	82.5
6526	87.1	88.4	90
6649	88.8	92.9	95
6845	91.4	100	102.5

\* 100% = 22,000 lbs (97,900 newtons) full scale

\*\* 100% = 16,000 lbs (71,200 newtons) full scale

These physical speeds were set in order to avoid shifting the frequency of the tones between 1/3 octave bands due to day to day ambient temperature variations.

Moreover, the following restrictions were imposed on acoustic testing:

1. Acoustic data were not taken with steady winds greater than 5 mph. (8.05 km/sec) or gusts greater than 3 mph. (4.83 km/sec);
2. Water or snow accumulation on the sound field prohibited testing;
3. Rain, snow or fog at the test site prohibited testing;
4. Testing was restricted to conditions where the relative humidity was greater than 30% and lower than 90%;
5. No absolute level acoustic data was taken while aerodynamic instrumentation was installed.

TABLE III.

QEP FAN B

TEST DATA ACCUMULATED ON SCALE MODEL  
TREATED AND UNTREATED WITH NOZZLE VARIATIONS

Run No.	Untreated Configurations				Treated Configurations			
	3	4	5	6	13	14	17	
Test Date	8/14/70							
Nozzle Size	8/17/70	8/20/70	8/21/70	8/24/70	9/19/70	9/19/70	10/6/70	
	Nom.	Large	Small	Nom.	Small	Large	Nom	
Fan Speed	Reading No's				Reading No's			
4040 RPM	19	39	60	--	218	--	261	
	23	44	67	--	229	--	271	
4474 (Approach)	20	40	61	--	219	239	262	
	24	45	68	--	230	244	272	
	21	42	62	--	220	--	263	
4700	25	46	69	--	231	--	273	
	22	43	63	--	221	240	264	
4907	26	47	70	--	232	245	274	
	27	48	64	--	222	--	265	
5505	30	51	71	--	233	--	275	
	28	49	65	--	223	241	266	
5990	31	52	72	--	234	246	276	
	29	50	66	--	224	--	267	
6354	32	53	73	--	235	--	277	
	33	54	74	79	226	242	268	
6526	34	56	--	82	236	247	278	
	--	55	75	80	227	--	269	
6649	--	57	77	83	237	--	279	
	--	58	76	81	228	243	270	
6845 (Take-off)	--	59	78	84	238	248	280	

Small nozzle = 372 in<sup>2</sup> (.24 m<sup>2</sup>)Nom. nozzle = 396 in<sup>2</sup> (.26 m<sup>2</sup>)Large nozzle = 460 in<sup>2</sup> (.30 m<sup>2</sup>)



## VI. Acoustic Data Reduction & Acoustic Scaling Procedure

### A. One Third Octave Data

The acoustic data reduction system, schematically illustrated in Figure 8, was designed specifically to perform time-averaged spectral analysis using a 30 second averaging time with a 1/3 octave bandwidth parallel filter system. Data was recorded on FM analog magnetic tape. This tape was played back through an amplifier/attenuator to provide the optimum signal input level to utilize the 50 dB dynamic range of the 1/3 octave filter system. The output of each filter was directly connected to a detector/integrator circuit which had built-in "hold" capabilities. The "hold" capability enabled the system to accumulate average signal amplitudes for each of the 1/3 octave bands and to hold them until they were processed through the analog-to-digital converter. The digital signal was then input to the DDP-116 Computer which provided a digital magnetic tape used for further computations and an on-line "quick-look" printout of sound pressure level spectra (temperature and humidity corrected to Standard Day). The "quick-look" information was used as a quality check prior to additional data reduction.

Additional data reduction included "Standard Data Reduction" and "Scaled Data." The former consisted of PNL, OASPL, PWL, OAPWL and D.I., as well as extrapolations to various sideline distances via the DDP-116 Computer. The latter, used for scale model data, provided the same type of data for both scale model and scale model projected to full size by methods described in the following section.

The 1/3 octave scale model data used to prepare this report are presented in the Appendix, Section IX.

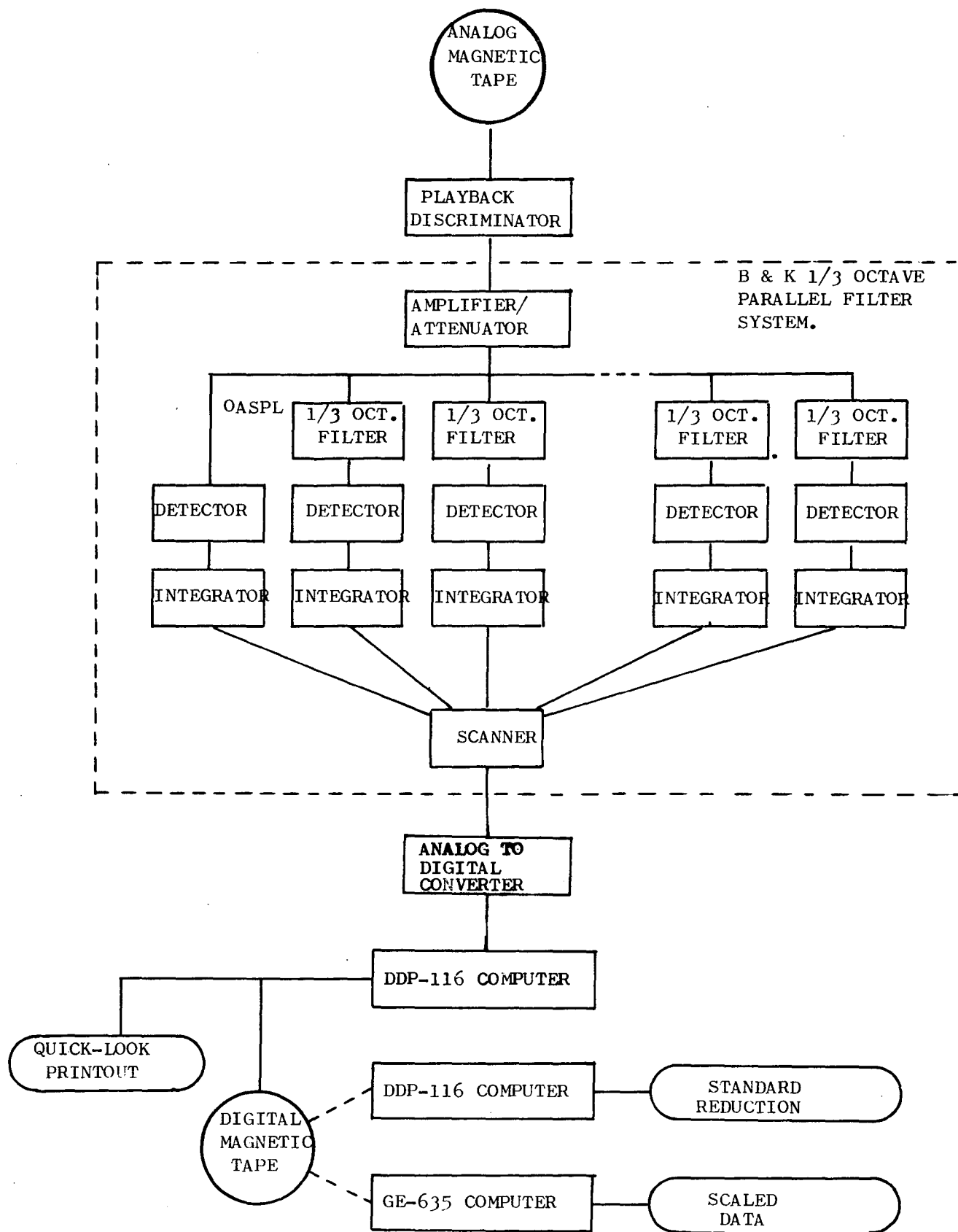


Figure 8

## B. Scaling Procedure

In addition to providing comparative data on noise reduction features, the scale model results were used to predict the full scale fan noise levels. In order to scale up the results, the frequency dependent atmospheric absorption corrections were removed from the scale model spectra to form an ideal spectra. This ideal spectra was then shifted as follows: the jet noise below the 1/3 octave band preceding the fundamental was shifted by the square root of the airflow ratio; the fan spectra were shifted by the ratio of the fan fundamental frequencies; and, a size adjustment of  $10 \log_{10}$  of the airflow ratio was added to all frequencies. The resulting spectra were then extrapolated, using the attenuations of the shifted frequencies, to various arc and sideline distances.

For example:

### 1. Adjustment for Fan Frequency Shift

Fundamental Frequency = Number of blades x RPM/60

$$f_1 \text{ scale model} = 26 \times 6845/60 = 2970 \text{ Hz}$$

$$f_1 \text{ full scale} = 26 \times 3320/60 = 1440 \text{ Hz}$$

The scale model fundamental appeared in the 3150 Hz 1/3 O.B. The full scale fundamental appeared in the 1600 Hz 1/3 O.B. Hence, the fan spectra was shifted three 1/3 octave bands.

### 2. Adjustment for Jet Noise Frequency Shift

$$\begin{aligned} \text{Shift factor} &= \sqrt{\text{airflow ratio}} = \sqrt{\frac{\text{flow, full scale}}{\text{flow, scale model}}} \\ &= \sqrt{4.26} \\ &= 2.07 \end{aligned}$$

Therefore, levels at 200 Hz were shifted by  $200/2.07$  to 97 Hz or to the 100 Hz  $1/3$  octave band. Thus, the jet noise was shifted three  $1/3$  octave bands.

### 3. Adjustment for Size

To account for the size difference, a general adder of  $10 \log_{10}$  airflow ratio or  $10 \log_{10} 4.26 = 6.3$  dB, was added at all frequencies.

### 4. Adjustment for Atmospheric Absorption

The model spectrum data was increased by an atmospheric absorption number (which increases with frequency) before frequencies were shifted for scaling. After shifting, atmospheric absorption numbers for the shifted frequencies were subtracted to account for the fact that the shifted frequencies showed less absorption.

Table V shows the scaling technique applied to a typical scale model spectra.

### C. Narrow Band Data

Narrow Band frequency analysis was performed by means of a Federal Scientific Ubiquitous Spectrum Analyzer, Model UA-6A, in conjunction with an Option 12913 High Resolution Digital Averager. The analyzer was capable of Fourier-analyzing all frequencies, within a selected frequency range, in real time. This analysis could be performed on continuous and intermittent signals as well as one time transients.

TABLE IV  
QEP FAN B  
SCALE MODEL  
SCALING TECHNIQUE

1/3 Octave Band Center Frequency (Hz)	① Scale Model 100' (30.5m) Arc W/Std. Day Corr.	② Atmospheric Attenuation per 100' (30.5m)	③ ① + ②	④ Shifted Spectra	⑤ ④ + 6.3 dB Weight flow Adder=6.3 dB	⑥ ⑤ - ② Full Scale Spectra 100' (30.5m) Arc W/Std. Day Corr.
50	82.0	0	82.0	83.8	90.1	90.1
63	84.1	0	84.1	83.3	89.6	89.6
80	83.2	0	83.2	80.7	87.3	87.3
100	83.8	0	83.8	84.7	91.0	91.0
125	83.3	0	83.3	89.3	95.6	95.6
160	80.7	0	80.7	91.9	98.2	98.2
200	84.7	0	84.7	89.3	95.6	95.6
250	89.3	0	89.3	86.2	92.5	92.5
315	91.9	0	91.9	88.7	95.0	95.0
400	89.2	.1	89.3	86.3	92.6	92.5
500	86.1	.1	86.2	87.7	94.0	93.9
630	88.6	.1	88.7	86.5	92.8	92.7
800	86.2	.1	86.3	87.8	94.1	94.0
1000	87.6	.1	87.7	86.5	92.8	92.7
1250	86.3	.2	86.5	86.2	92.5	92.3
1600	87.6	.2	87.8	91.7	98.0	97.8
2000	86.2	.3	86.5	88.7	95.0	94.7
2500	85.8	.4	86.2	89.8	96.1	95.7
3150	91.2	.5	91.7	93.2	99.5	99.0
4000	88.0	.7	88.7	90.8	97.1	96.4
5000	88.9	.8	89.8	89.1	95.4	94.5
6300	92.0	1.2	93.2	87.5	93.8	92.6
8000	89.1	1.7	90.8	84.9	91.2	89.5
10000	86.6	2.5	89.1	84.5	90.8	88.3
12500	83.6	3.9	87.5			
16000	79.0	5.9	84.9			
20000	76.0	8.5	84.5			

114.7 PNdB

121.7 PNdB

The Averager accumulated the short-term spectra (produced by the Ubiquitous Analyzer) and obtained the mean spectrum characteristics in real time. Successive spectra were summed digitally over a selected period of time and the resultant average was displayed via an X-Y plotter. Averaging resulted in signal-to-noise ratio enhancement and was useful for detecting spectrum components which are "buried" in noise.

Narrow Band analysis performed for this report consisted of a frequency range of 20 to 10K Hz with a nominal filter band width of 20 Hz. The integration time used was 12.8 seconds, with 256 scans during this time period.

## VII. ACOUSTIC DATA ANALYSIS

### A. NOISE VARIATIONS WITH SPEED

Figures 9 - 13 show the noise characteristics at several speeds for the untreated configuration of scale model Fan B with the nominal nozzle. The data presented were recorded around a 100 foot (30.5 m) arc and have been corrected to Standard Day conditions of 59°F (15°C) temperature and 70% relative humidity.

Figures 9 and 10 show the distribution of the fundamental and second harmonic respectfully around the arc at approach and takeoff thrust. The SPL's of the tones were derived from narrowband data and then corrected to Standard Day. The sound power levels were calculated from these arc SPL values. The fundamental at approach was 10.7 dB PWL lower than at takeoff and the second harmonic was 8.5 dB PWL lower at approach than at takeoff thrust. The maximum fundamental tones occurred in the front quadrant for both takeoff and approach thrusts while the maximum second harmonic occurred in the rear quadrant for both power settings.

Figures 11 and 12 present the 1/3 octave spectrum at 50° and 120° respectfully, for 60%, 70%, 80% and 90% corrected fan speeds. (The 1/3 octave scale model data is presented in the Appendix for all angles). Although the blade passing frequency occurred in different 1/3 octave bands for different fan speeds, it can be seen that the fundamental increased with increasing speed at both angles. Further, the noise level below 1600 Hz generally increased with speed.

The second harmonics likewise increased with increasing speed with the exception of the one at  $50^\circ$  for  $90\%N_{f_c}$  which was lower than the second harmonics for this angle at  $70\%$  and  $80\%N_{f_c}$ . Note that the difference between  $60\%$  and  $70\%$  speeds was markedly greater than between any other pair of adjacent speeds.

Figure 13 contains sound power level spectra versus frequency for the four speeds. Again, it can be seen that the levels of the tones and the broadband noise increased with increasing speed. Note the  $60\%N_{f_c}$  PWL was quite a bit lower than the  $70\%N_{f_c}$  PWL while the  $70\%$ ,  $80\%$  and  $90\%$  PWL's were rather closely grouped - approximately 7 dB difference between the  $60\%$  and  $70\%$  fundamental while only  $2\frac{1}{2}$  dB between the  $70\%$  and  $90\%$  fundamental.



SCALE MODEL FAN B  
FUNDAMENTAL - STANDARD DAY

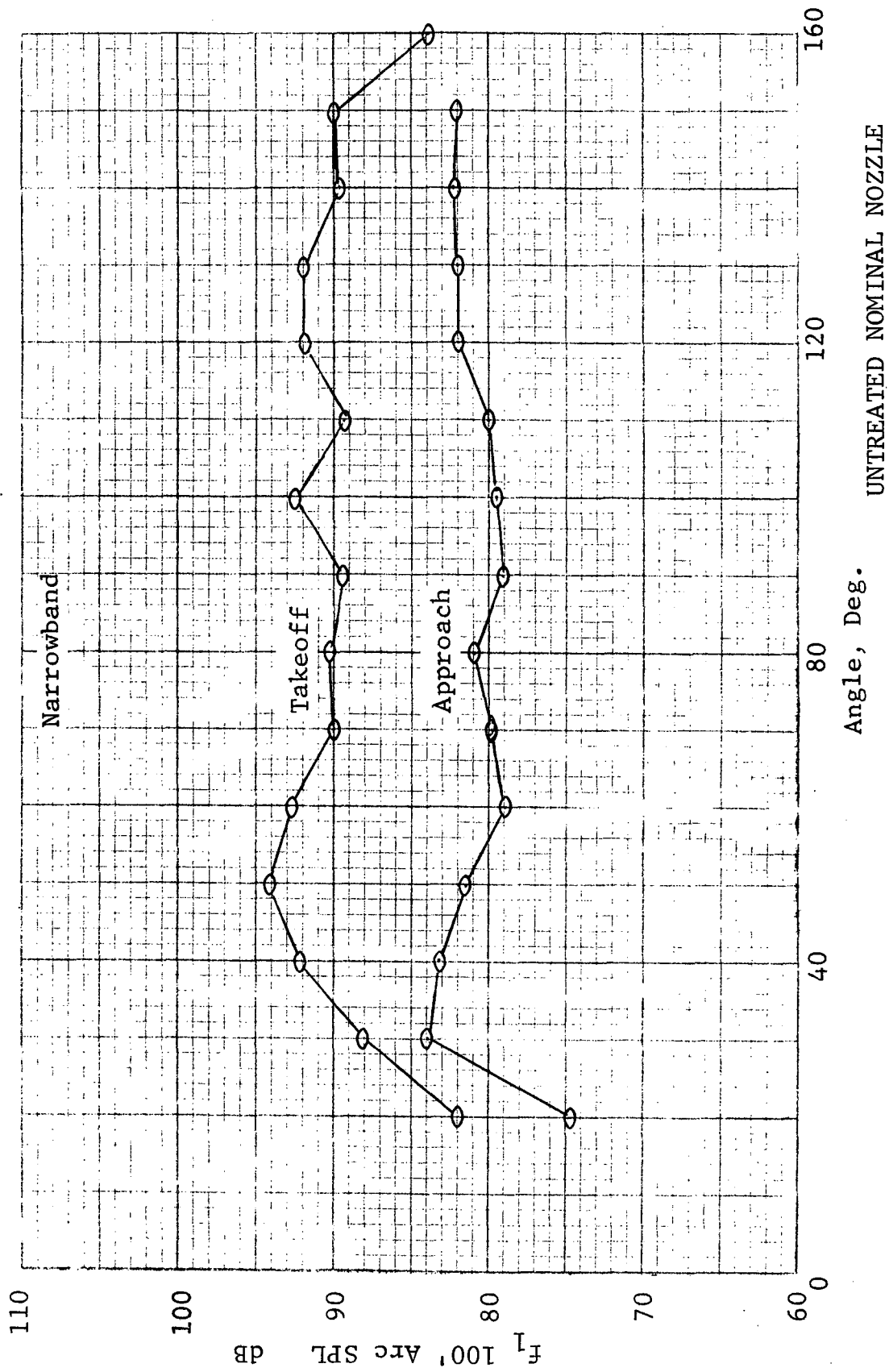


Figure 9

Approach - PWL=131.5 dB  
Takeoff - PWL=142.2 dB

SCALE MODEL FAN B  
SECOND HARMONIC - STANDARD DAY

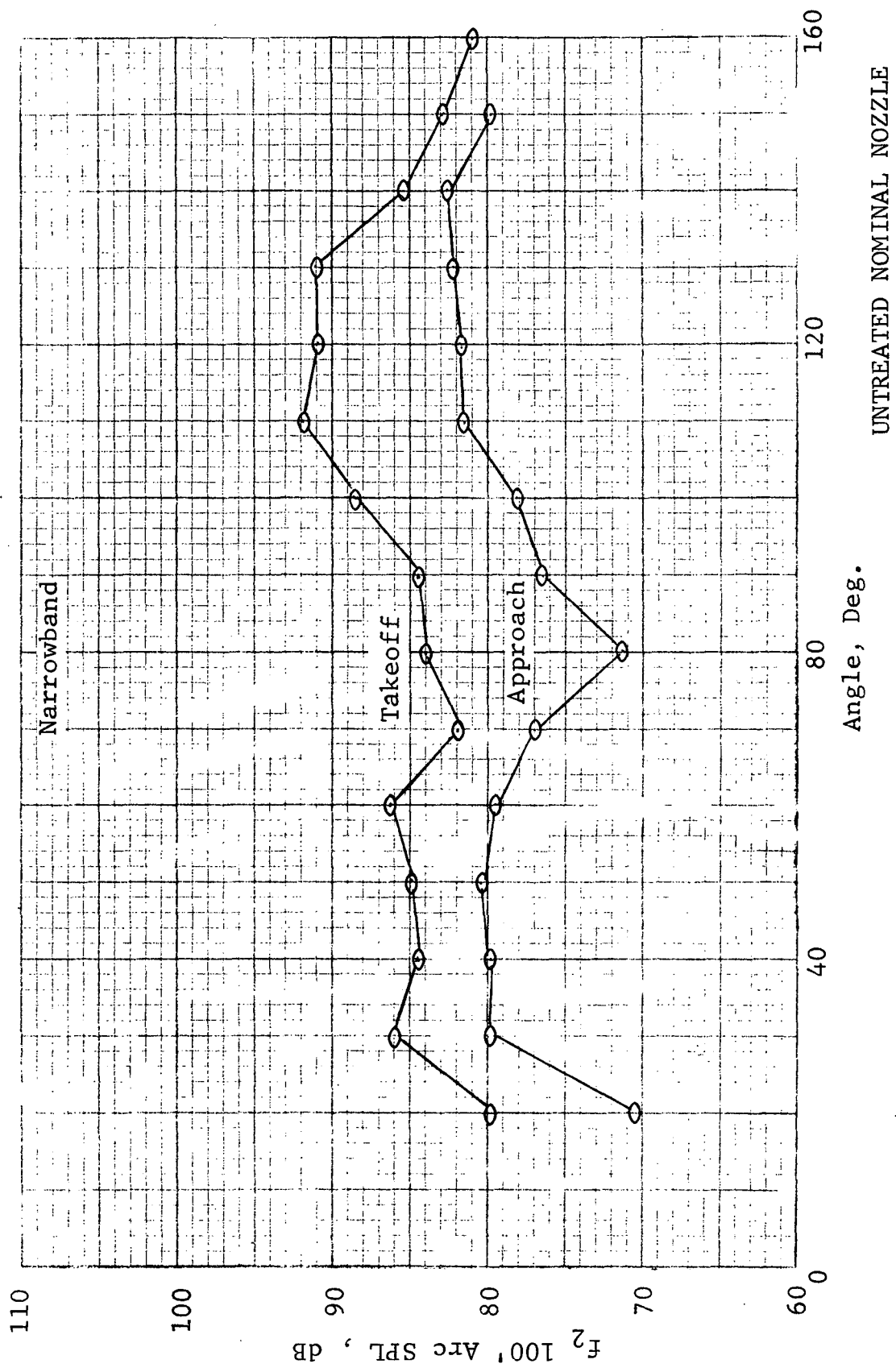


Figure 10

Approach - PWL=130.7 dB  
Takeoff - PWL=139.5 dB

# QEP FAN B SCALE MODEL RESULTS

50°

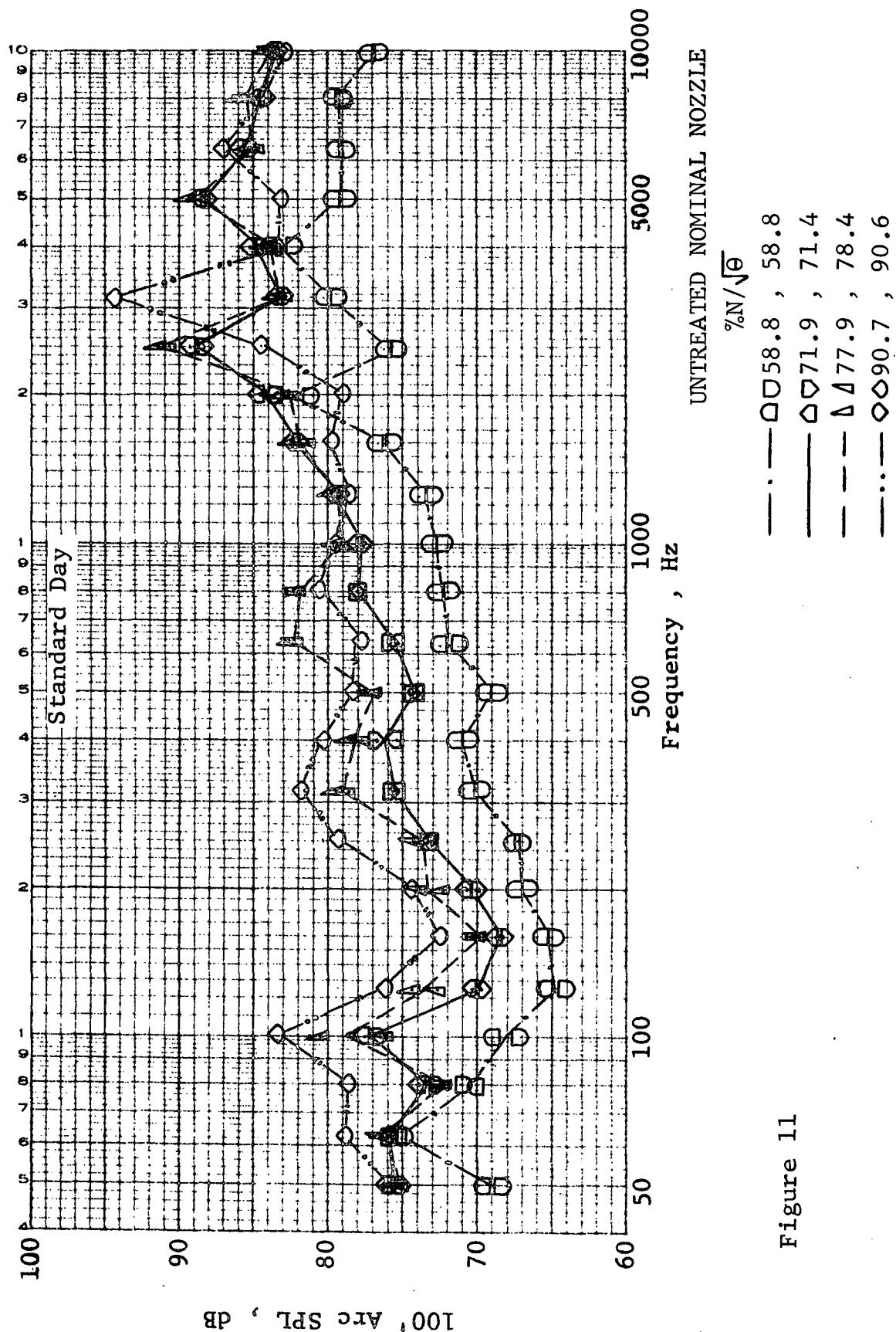


Figure 11

# QEP FAN B SCALE MODEL RESULTS

120°

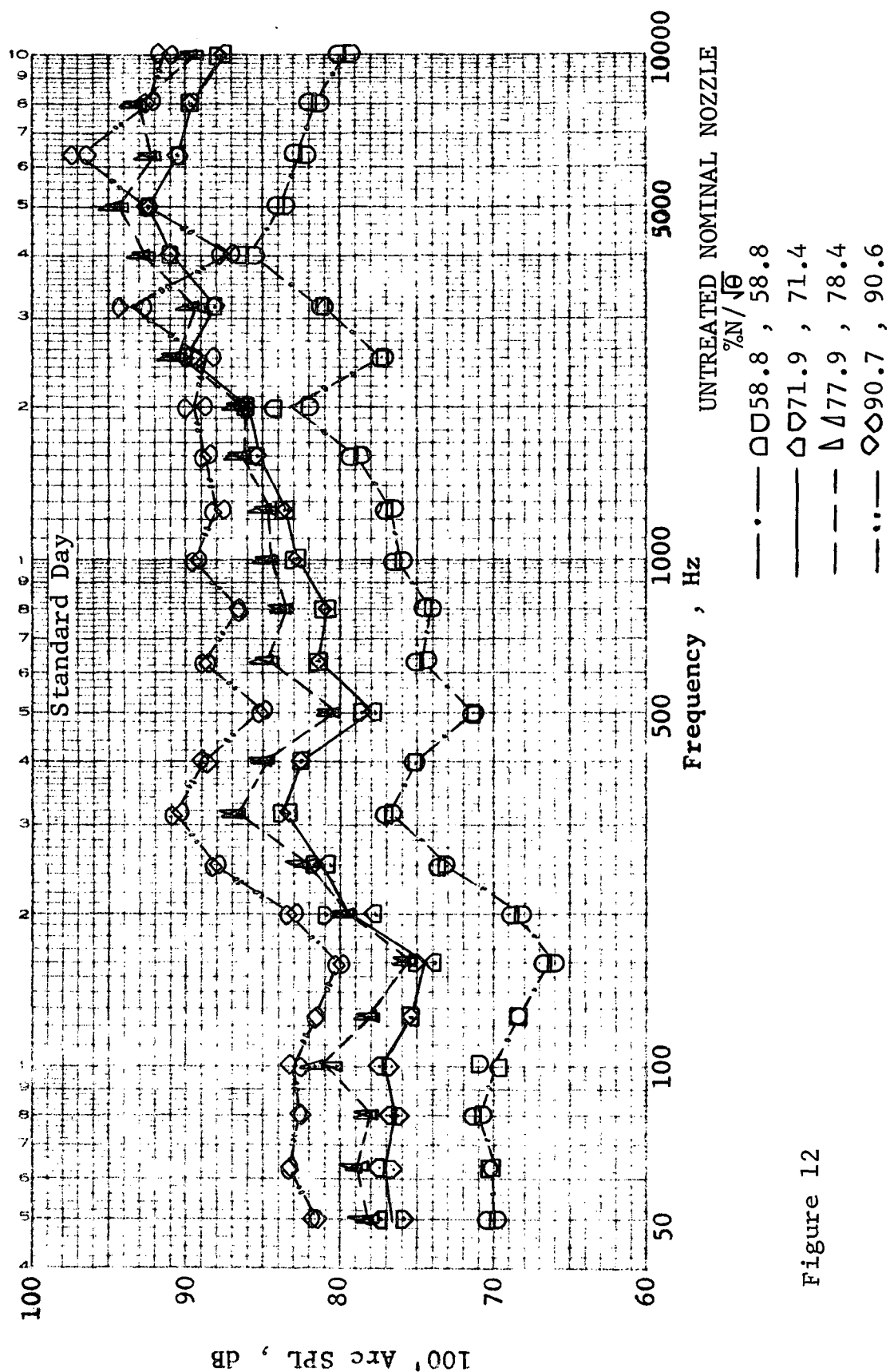


Figure 12

QEP FAN B SCALE MODEL RESULTS  
SOUND POWER LEVELS

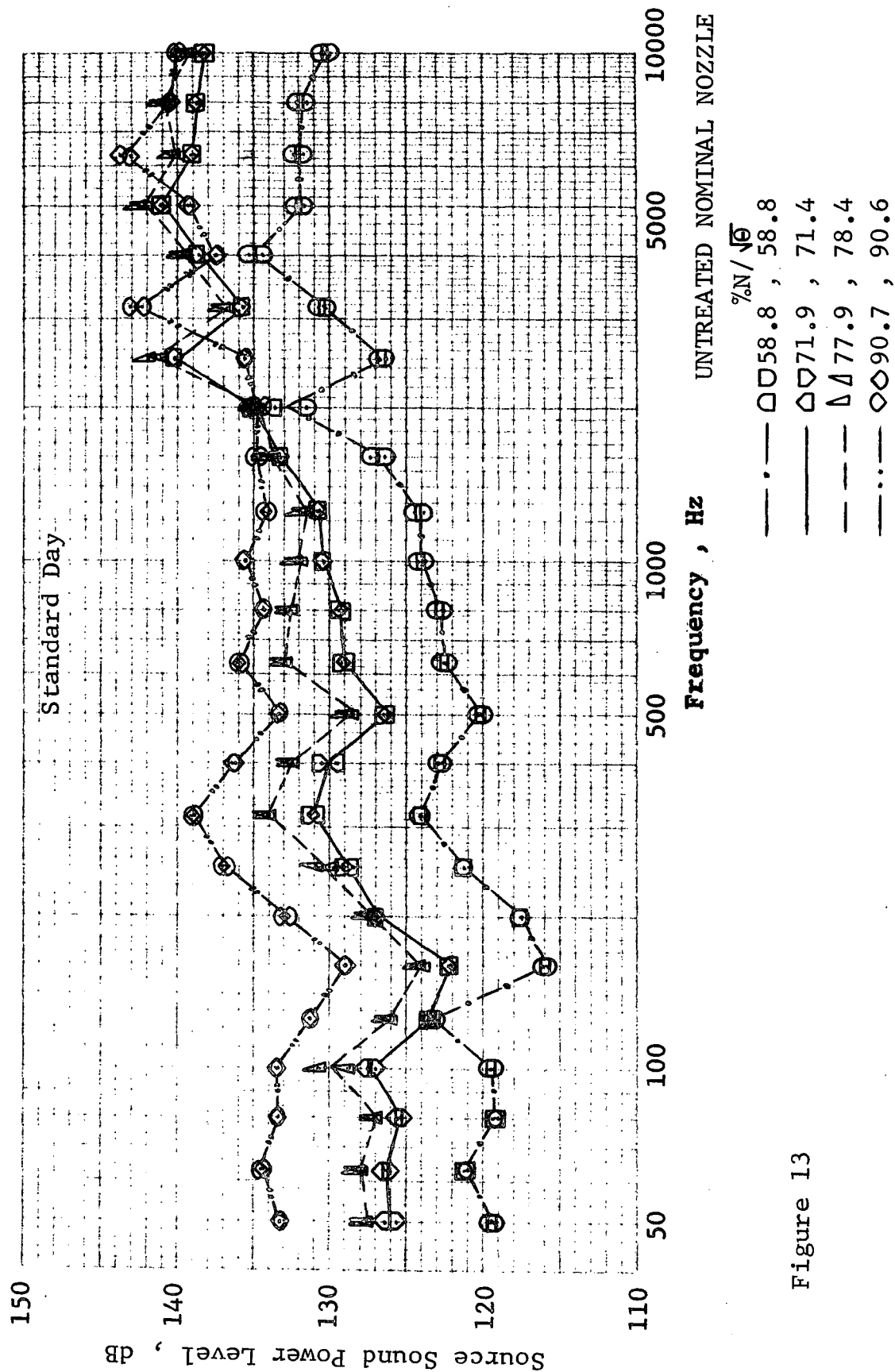


Figure 13

## B. NOISE VARIATIONS WITH FAN NOZZLE AREA

Figures 14 - 23 present the noise characteristics of the untreated scale model configuration at approach and takeoff thrusts with three different fan nozzles. These nozzles were designated small, 372 square inches ( $.24 \text{ m}^2$ ); nominal, 396 sq. inches ( $.26 \text{ m}^2$ ); and large, 460 sq. inches ( $.30 \text{ m}^2$ ). The data presented in these figures are for a 100 foot (30.5 m) arc.

The distribution around the arc of the fundamental and the second harmonic of the fan with three nozzles is shown in Figures 14 and 15 for approach thrust and in Figures 16 and 17 for takeoff thrust. The sound pressure levels of the tones were derived from narrowband data and these levels have been corrected to Standard Day conditions. In each of the four cases, the tone level of the large nozzle was the highest while that of the small nozzle was the lowest. The sound power level of the fundamental at approach differed by 2.1 dB PWL between the large and nominal nozzles and by 2.1 dB PWL between the nominal and small nozzles, respectively. The PWL of the second harmonic at approach was very similar for the large and nominal nozzles, while the small nozzle was 2.2 dB PWL lower than the nominal nozzle. However, at takeoff thrust, the PWL of the tones for the nominal and small nozzle were both similar amounts lower than the large nozzle. The maximum tones for each of the four cases occurred in the rear quadrant, although the rear to front quadrant difference is slight for the fundamental at approach.

The 1/3 octave spectra for approach thrust at  $50^\circ$  and  $120^\circ$  (Figures 18 and 19) likewise indicate that the tone levels of the small nozzle were less than those of the other nozzles. However, these figures also indicate that the broadband noise of the small nozzle was substantially higher than the broadband noise of the other nozzles from 315 Hz to 10 KHz at  $50^\circ$  and from 315 Hz to 2000 Hz at  $120^\circ$ . The broadband noise was generally higher for the small nozzle at takeoff thrust from 315 Hz to 10 KHz as well, as indicated by Figure 20 for  $50^\circ$  and by Figure 21 for  $120^\circ$ .

Figure 22 contains sound power levels versus frequency for the three nozzles at approach thrust. Again, the broadband noise for the small nozzle is shown to be significantly higher than the other two nozzles from 315 Hz to 4000 Hz. Figure 23 contains the PWL spectra at takeoff thrust for the three nozzles. The broadband noise was also higher at this thrust level for the small nozzle than for the other nozzles, although the difference was not as great as that at approach thrust.

QEP FAN B SCALE MODEL  
FUNDAMENTAL AT APPROACH  
STANDARD DAY NARROWBAND

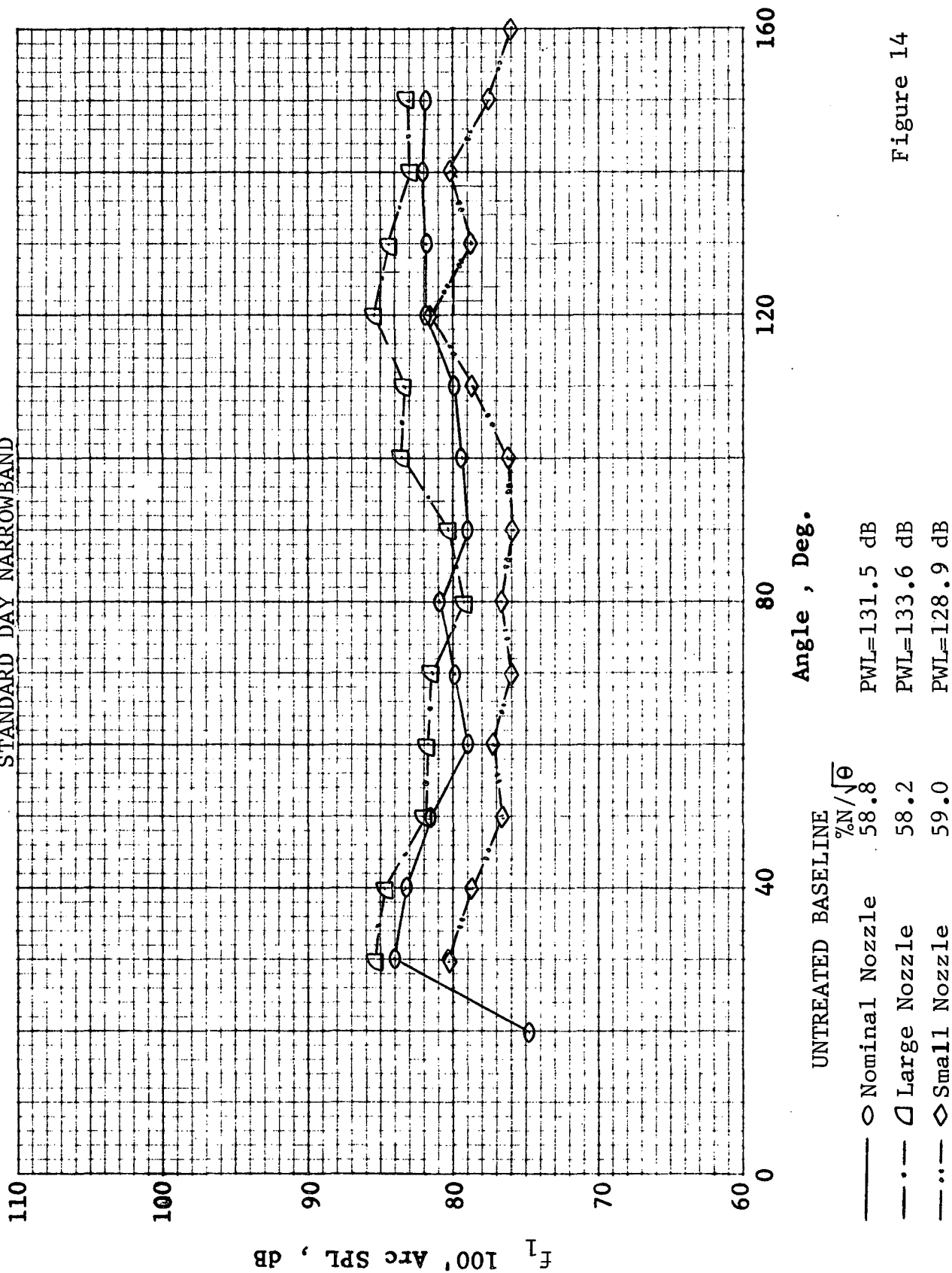


Figure 14



QEP FAN B SCALE MODEL  
SECOND HARMONIC AT APPROACH  
STANDARD DAY NARROWBAND

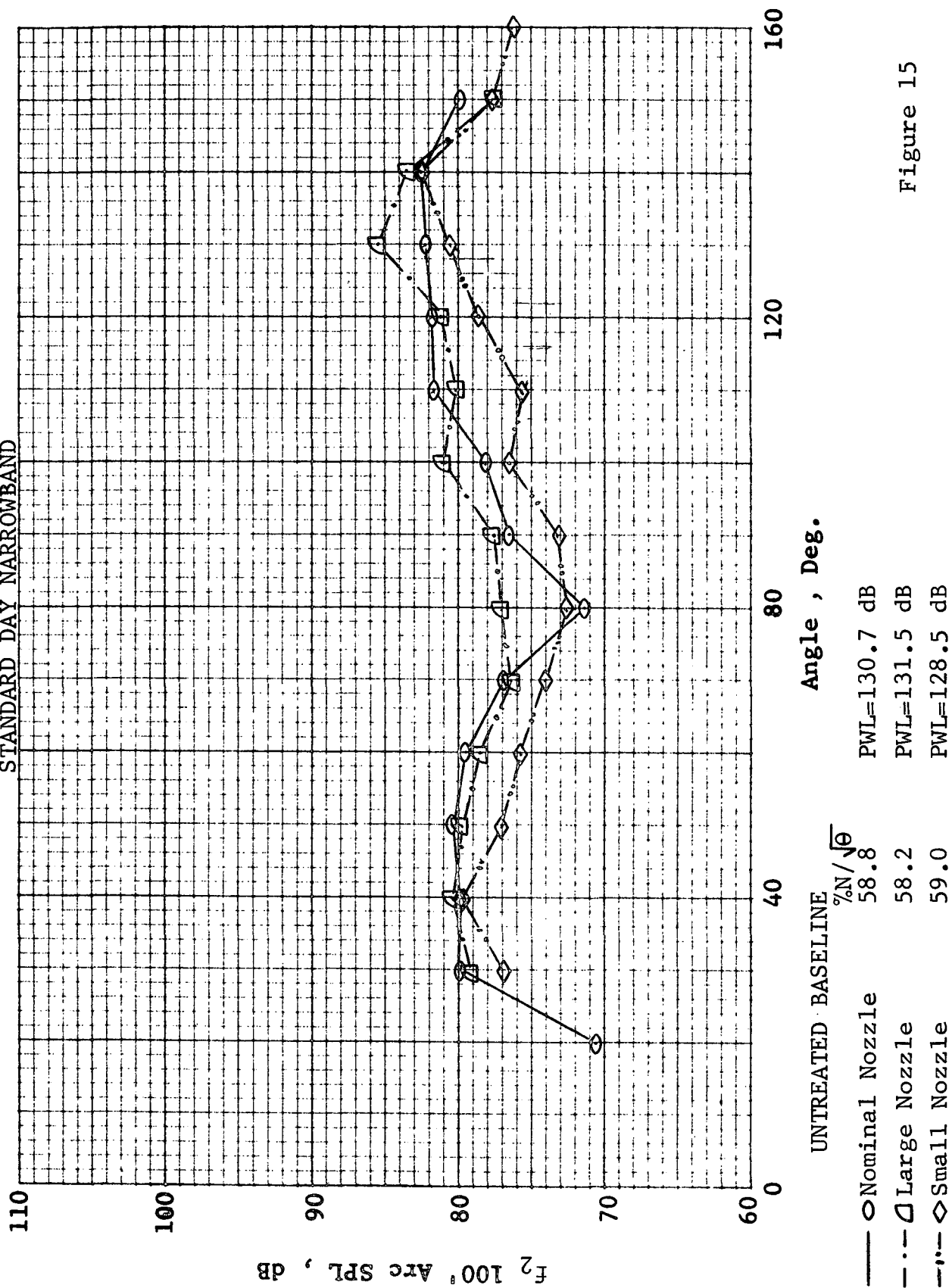


Figure 15

QEP FAN B SCALE MODEL  
FUNDAMENTAL AT TAKEOFF  
STANDARD DAY NARROWBAND

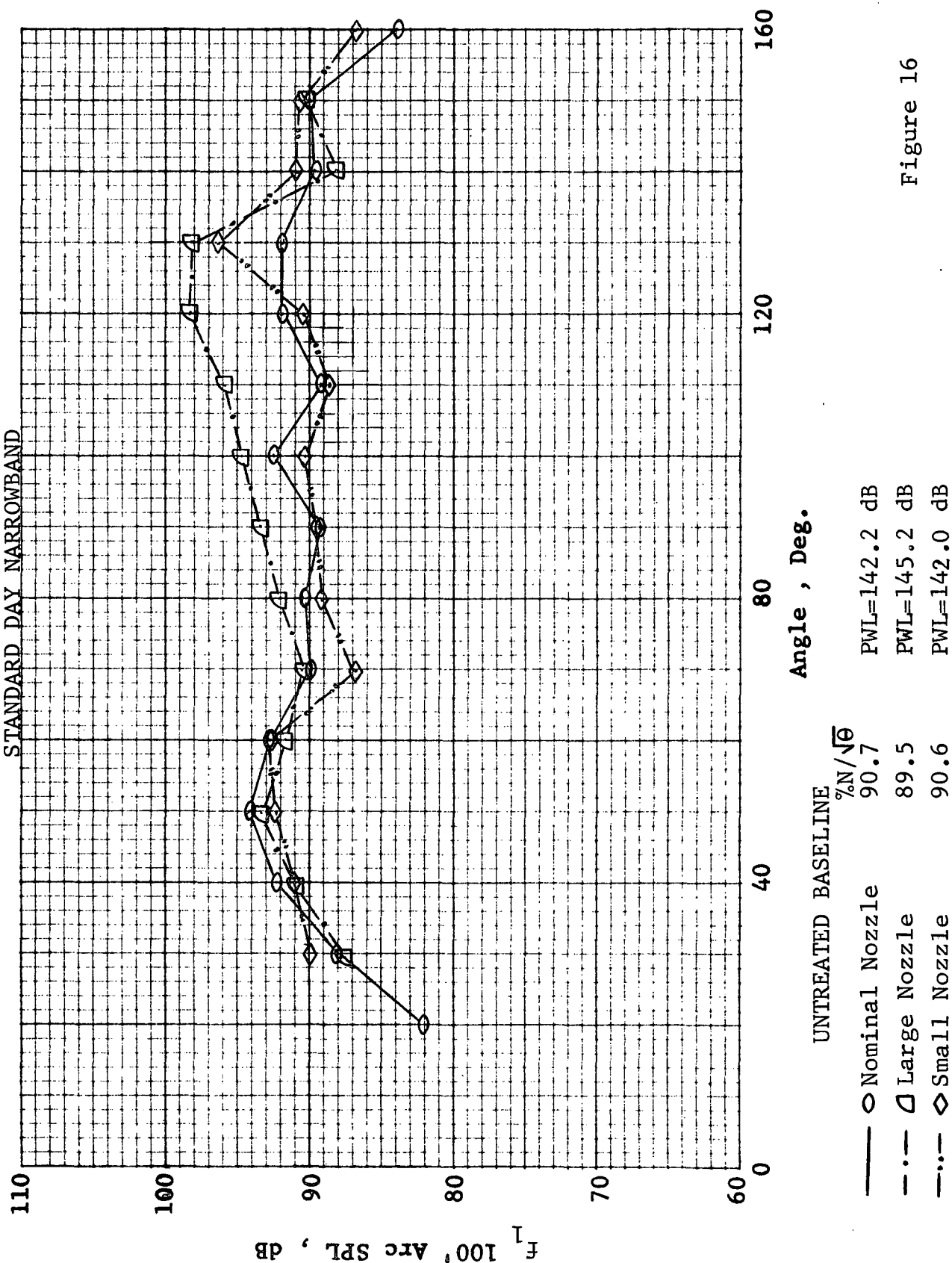


Figure 16

QEP FAN B SCALE MODEL  
SECOND HARMONIC AT TAKEOFF  
STANDARD DAY NARROWBAND

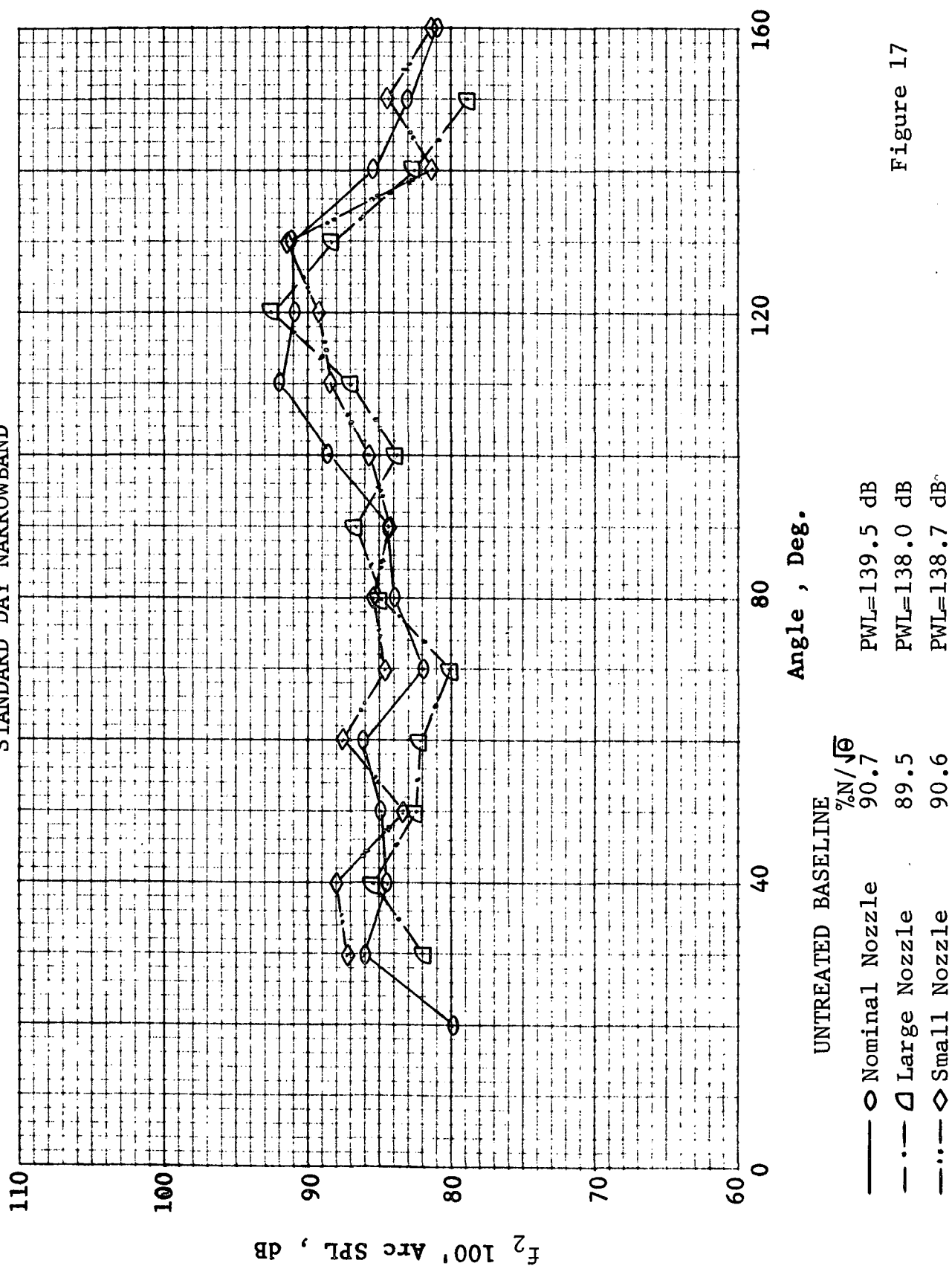


Figure 17

QEP FAN B SCALE MODEL RESULTS  
50° AT APPROACH

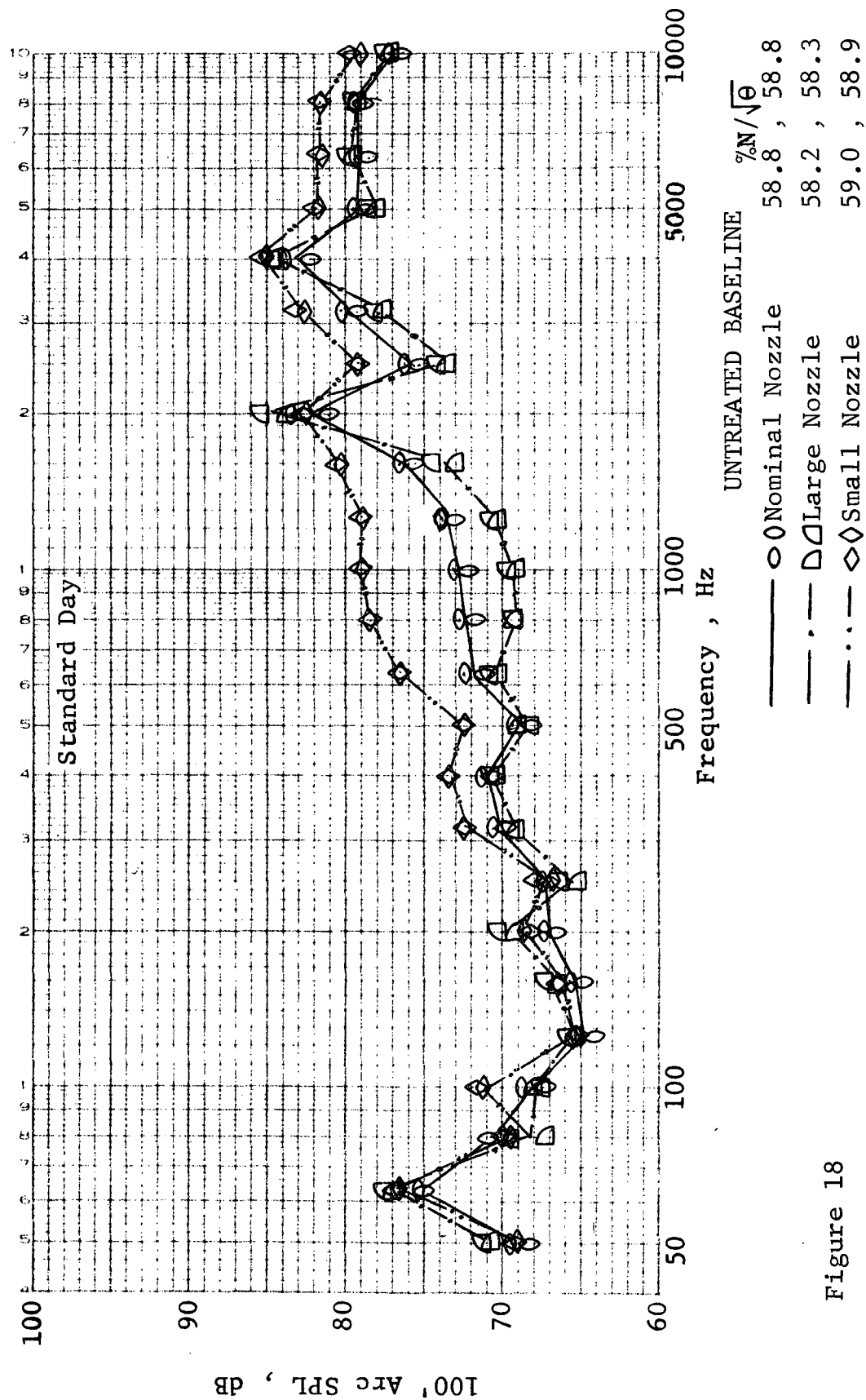


Figure 18

QEP FAN B SCALE MODEL RESULTS  
120° AT APPROACH

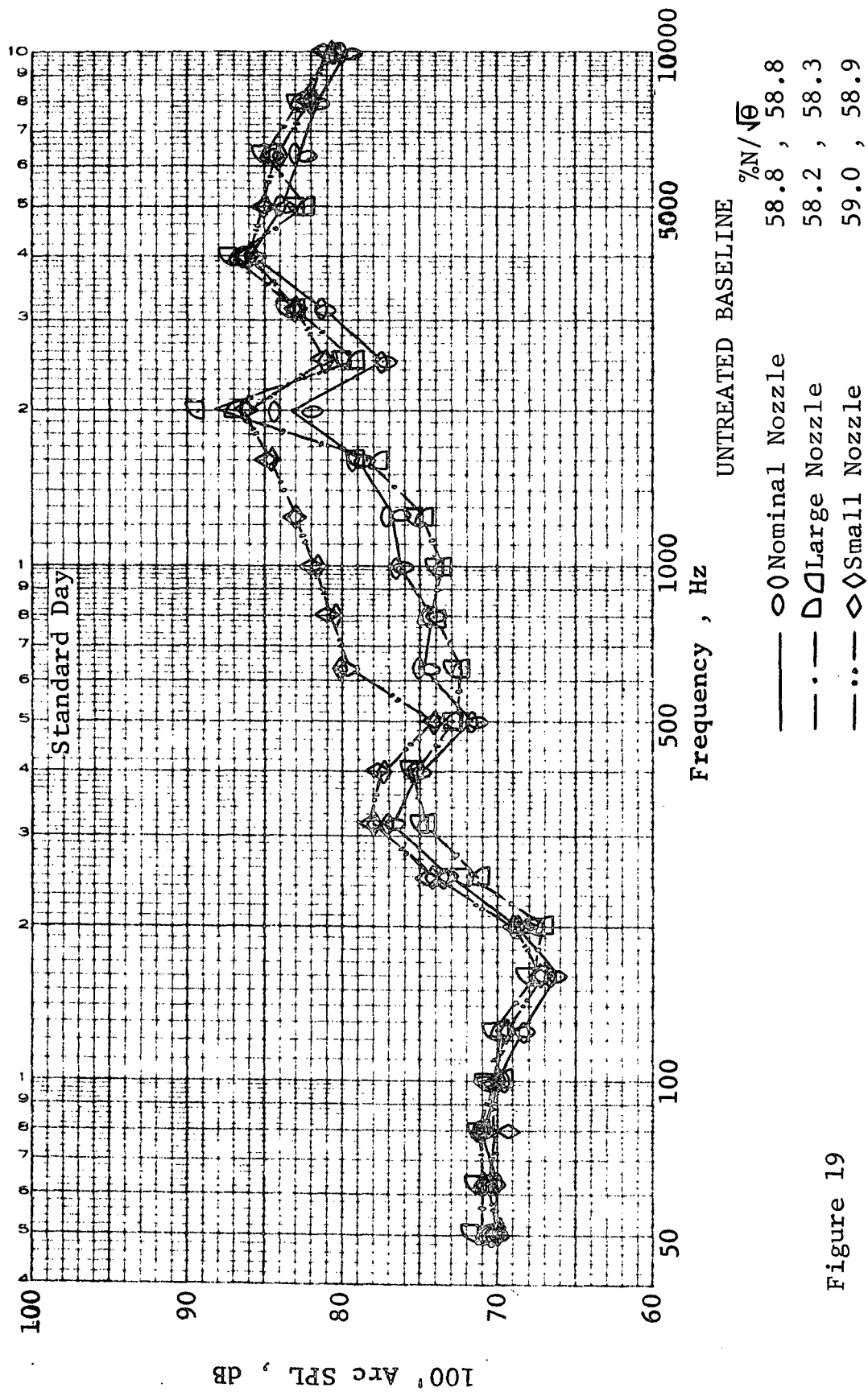


Figure 19

# QEP FAN B SCALE MODEL RESULTS

50° AT TAKEOFF

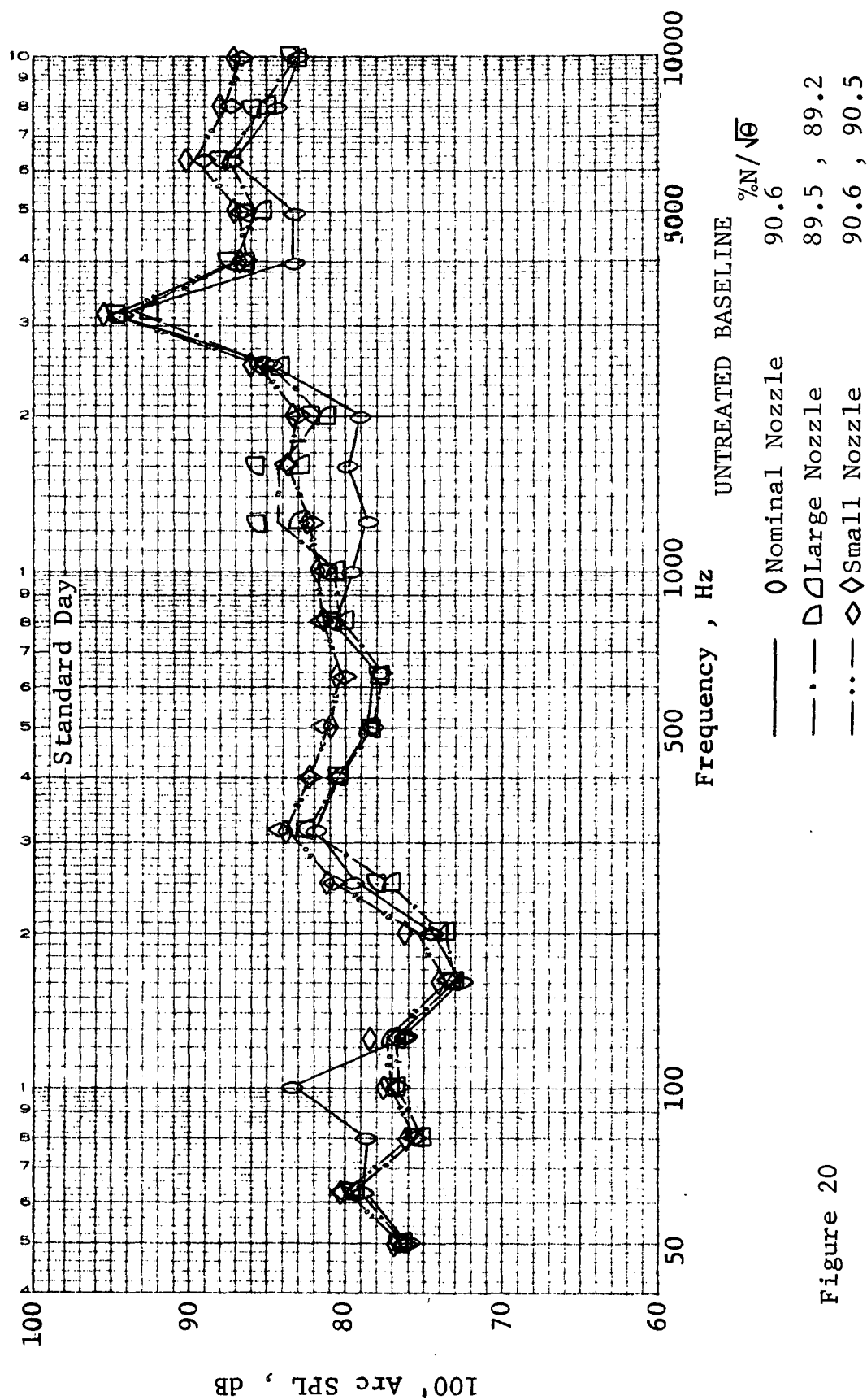


Figure 20

QEP FAN B SCALE MODEL RESULTS  
120° AT TAKEOFF

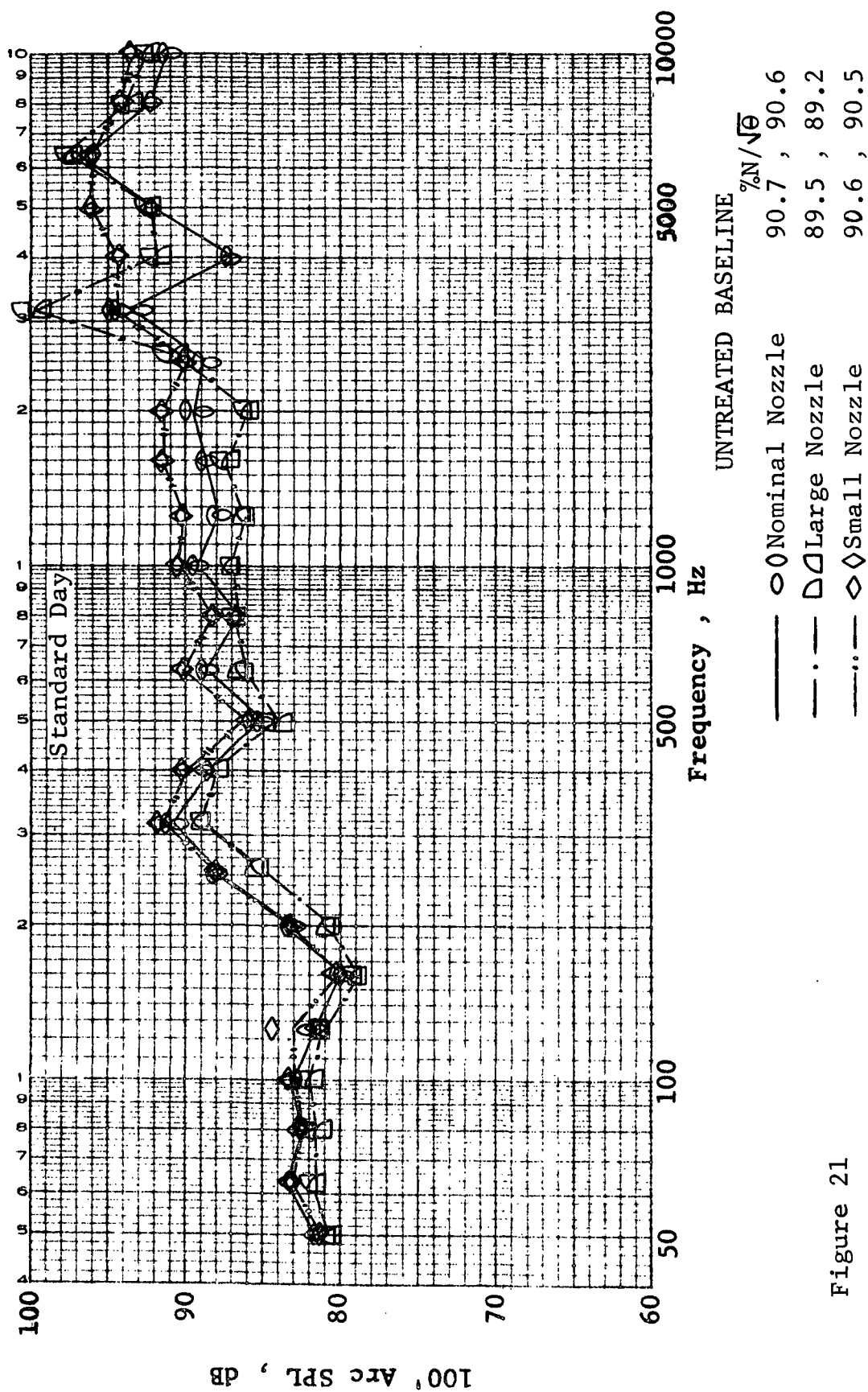


Figure 21

QEP FAN B SCALE MODEL RESULTS  
SOUND POWER LEVELS AT APPROACH

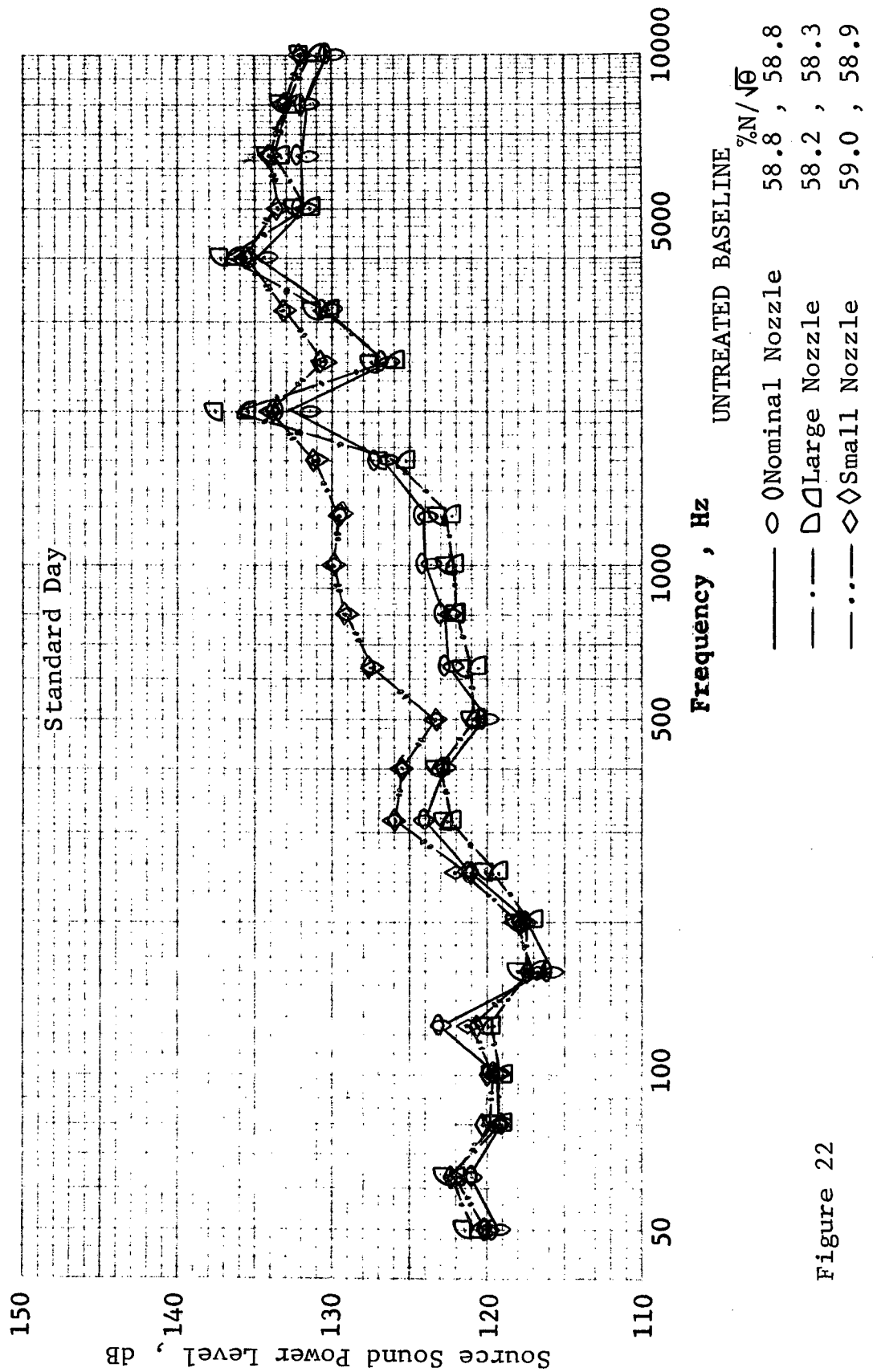


Figure 22



QEP FAN B SCALE MODEL RESULTS  
SOUND POWER LEVELS AT TAKEOFF

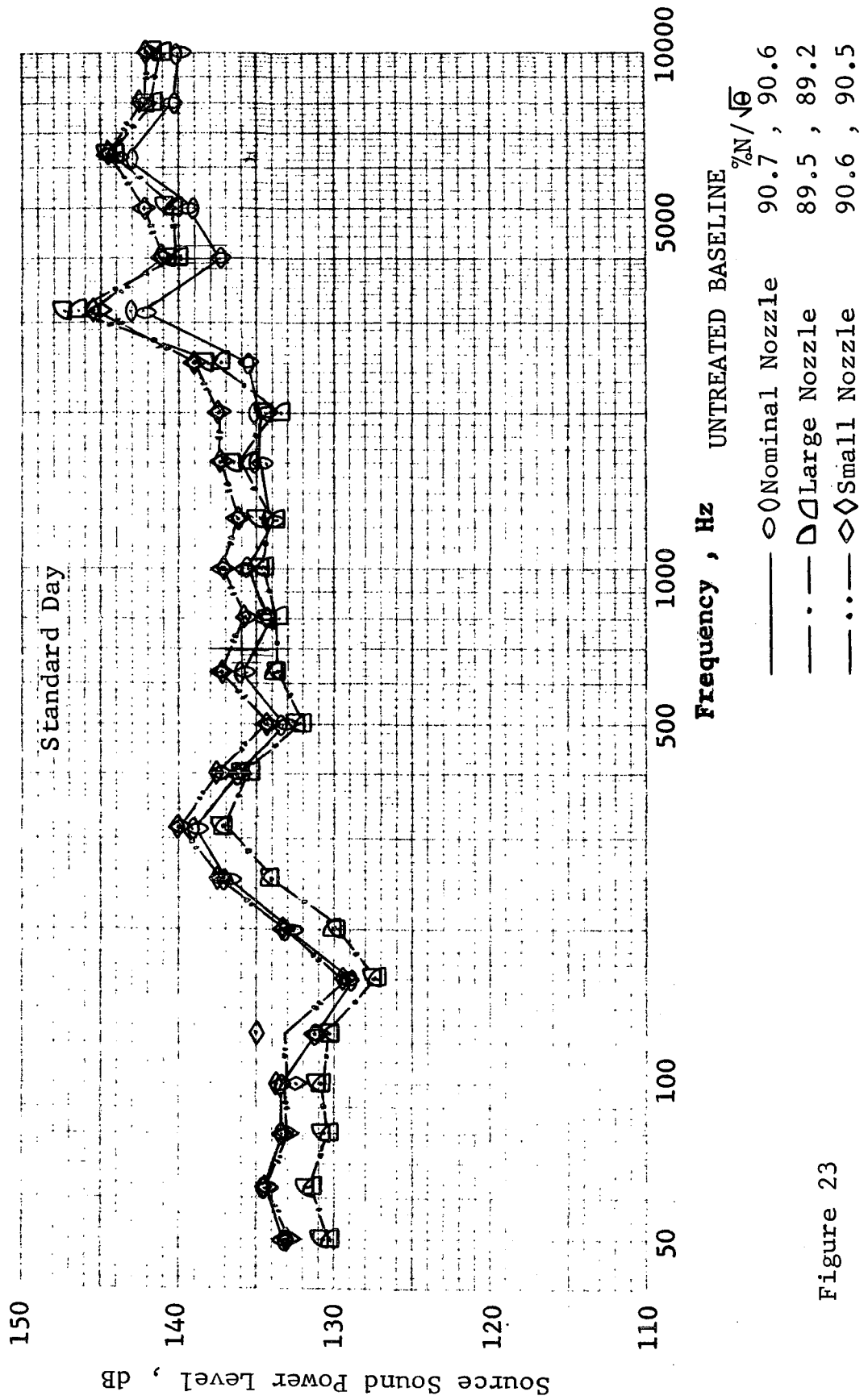


Figure 23

### C. ACOUSTIC TREATMENT EFFECTS

Comparisons of the untreated and the treated configurations of the scale model fan with the nominal nozzle are presented in Figures 24 - 33. The acoustic treatment of the frame area is described in the Test Vehicle Description, Section IV. To produce the untreated configuration, this acoustic treatment was neutralized by covering it with tape.

Figures 24 - 27 show the distribution of the fundamental and second harmonic around the 100 foot (30.5 m) arc as derived from narrowband data which have been corrected to Standard Day conditions. At approach thrust, (Figures 24 and 25), both tones have been significantly reduced due to the acoustic treatment - the fundamental by 4.5 dB PWL and the second harmonic by 5.2 dB PWL. The fundamental reduction was noticeable around most of the arc while the second harmonic reduction was most significant in the aft quadrant. At takeoff thrust, the tones also showed a noise decrease in the aft quadrant, however, the fundamental showed a noise increase in the front quadrant. Figure 26 shows a split PWL, computed by segmenting the arc into front quadrant at angles less than 85 degrees and aft quadrant at angles greater than 85 degrees. The front fundamental noise increased by 3.8 dB PWL while the aft decreased 1.9 dB PWL. The total, accordingly, showed an increase with treatment. In the case of the second harmonic, (Figure 27), there was a sizable decrease of 5.8 dB PWL in the aft quadrant but effectively no change in the front.

The one third octave data clearly indicates that not only have the tones been reduced at approach thrust but the broadband noise between the tones has been decreased as well by the acoustic treatment.

At  $50^\circ$  (Figure 28), the greatest reduction occurred in the 2500 Hz and 3150 Hz bands. At  $120^\circ$  (Figure 29), the broadband noise was decreased 5 dB or more from 2 to 10 KHz. The  $120^\circ$  results for takeoff thrust indicate similar broadband noise reductions for the treated configuration as indicated in Figure 31. However, the 1/3 octave data at  $50^\circ$  (Figure 30) indicates the broadband noise of the two configurations was generally the same across the spectrum except at 1600 Hz where the treated data shows some increase. Upon examination of narrowband data, this increase appears to be attributable to multiple pure tones occurring with the treated configuration. The present hypothesis is that this noise increase is attributed to the increase turbulence generated by the presence of the treatment close to the rotor.

Figure 32 contains the sound power level spectra for the two configurations at approach thrust, showing the noise reduction for the treated fan at the tones and for the broadband noise from 1.6 to 10 KHz. The PWL spectra for takeoff thrust (Figure 33) indicates less noise reduction of broadband noise and the second harmonic tone along with a 2 dB PWL increase at the fundamental tone.

SCALE MODEL FAN B  
FUNDAMENTAL AT APPROACH  
STANDARD DAY

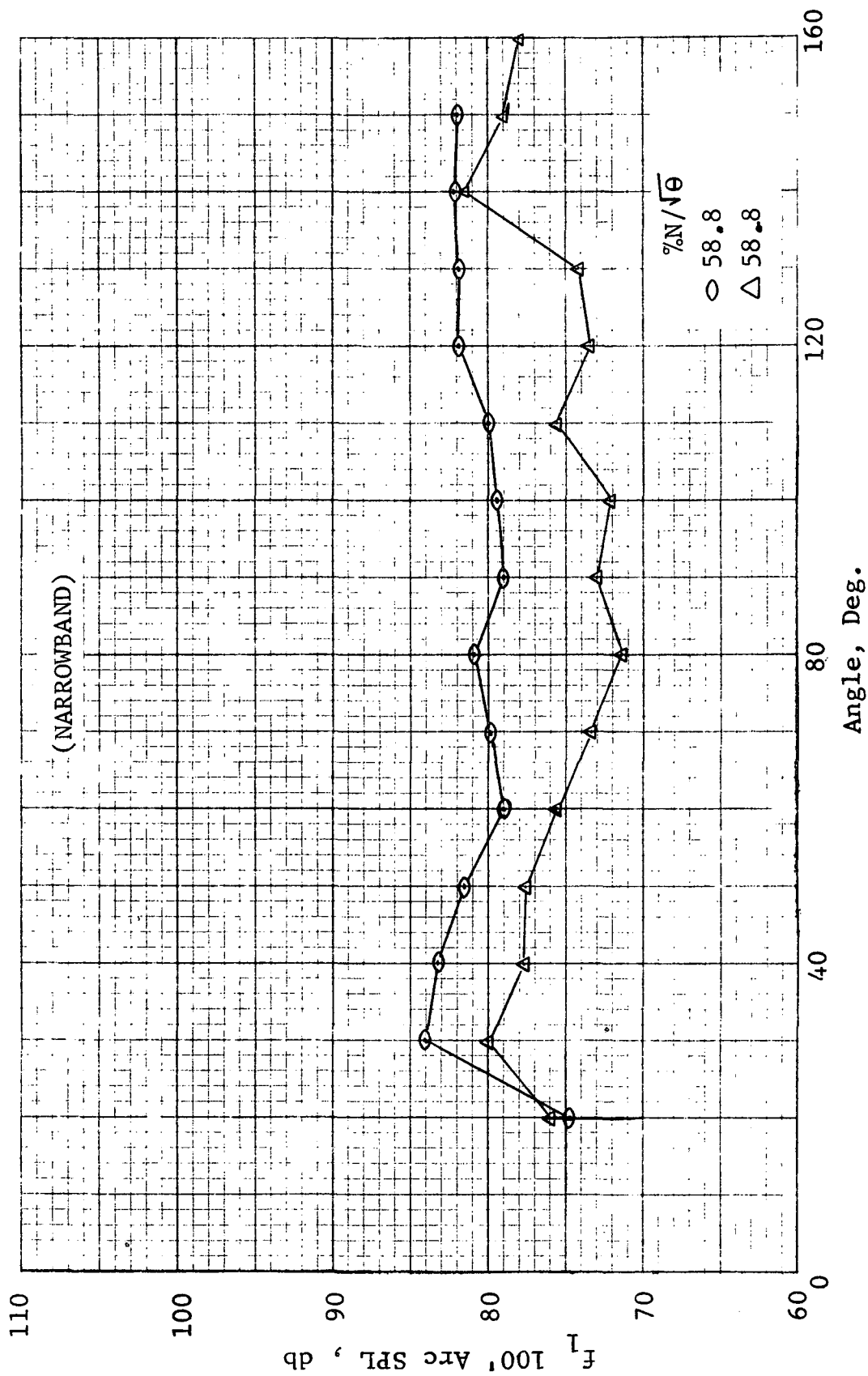


Figure 24

SCALE MODEL FAN B  
SECOND HARMONIC AT APPROACH

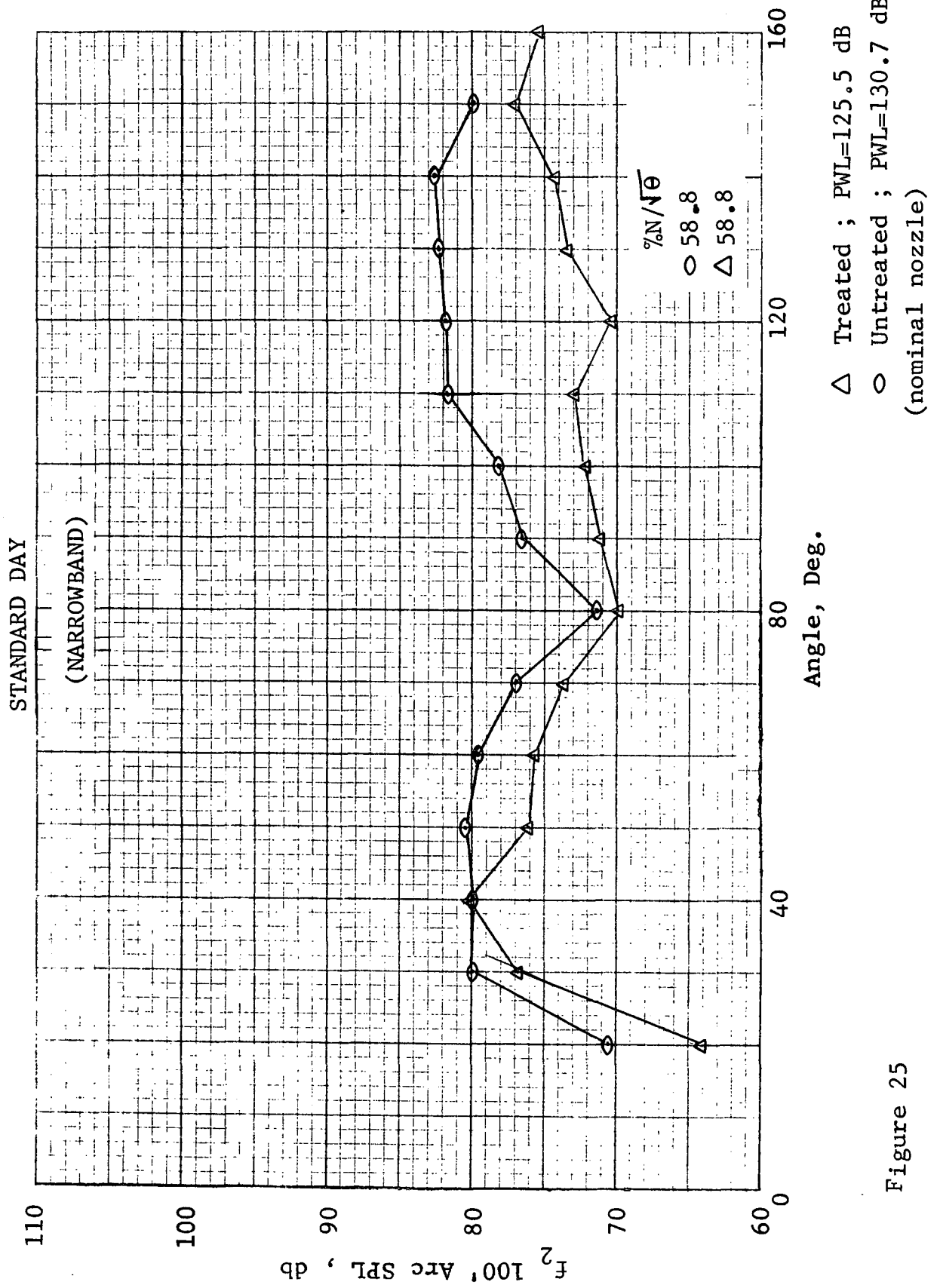


Figure 25

SCALE MODEL FAN B  
FUNDAMENTAL AT TAKEOFF  
STANDARD DAY

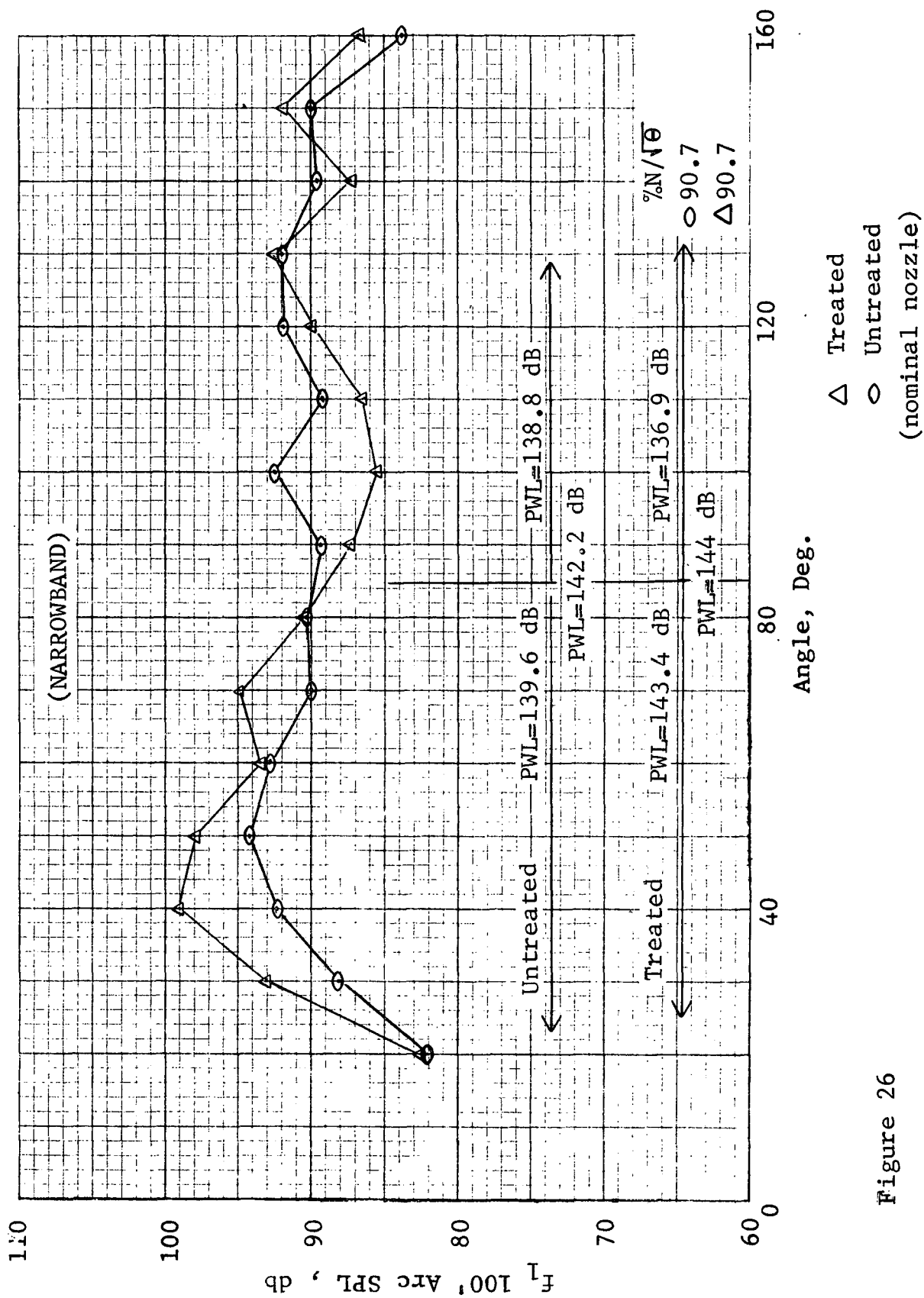


Figure 26

SCALE MODEL FAN B  
SECOND HARMONIC AT TAKEOFF

STANDARD DAY

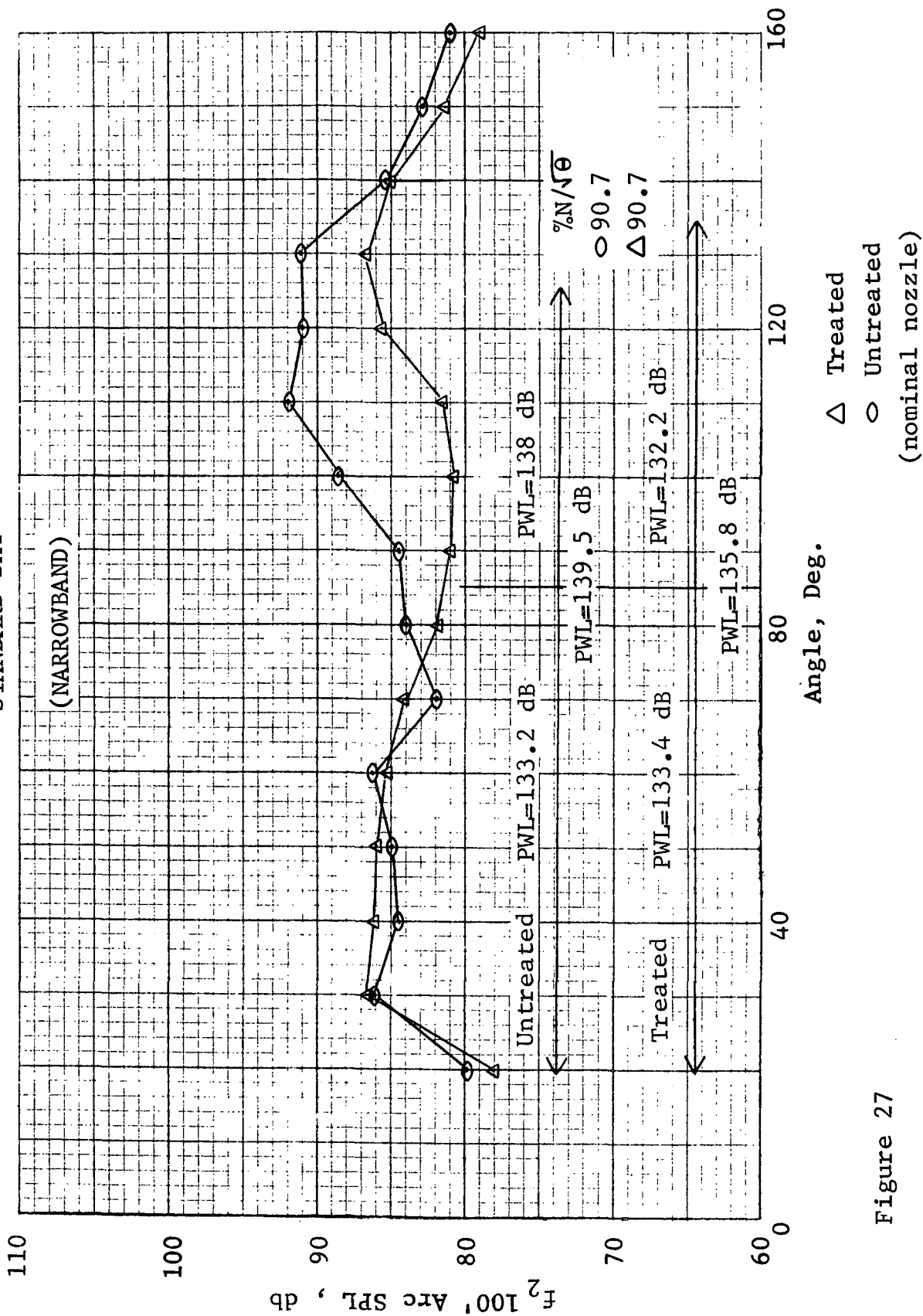


Figure 27

QEP FAN B  
SCALE MODEL RESULTS  
100' ARC SPL  
TREATED VS UNTREATED  
APPROACH

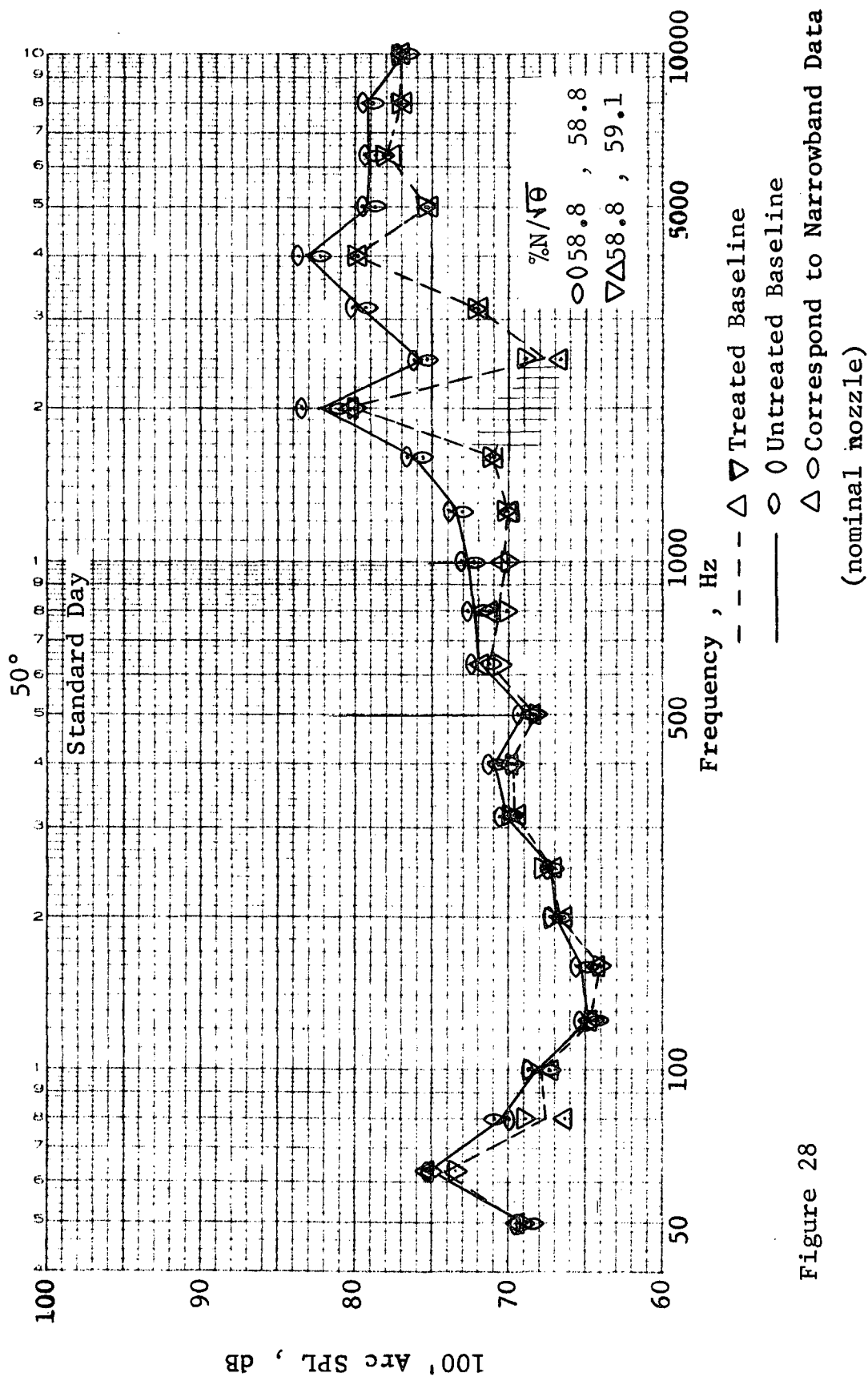


Figure 28



QEP FAN B  
SCALE MODEL RESULTS  
100' ARC SPL  
TREATED VS UNTREATED  
APPROACH

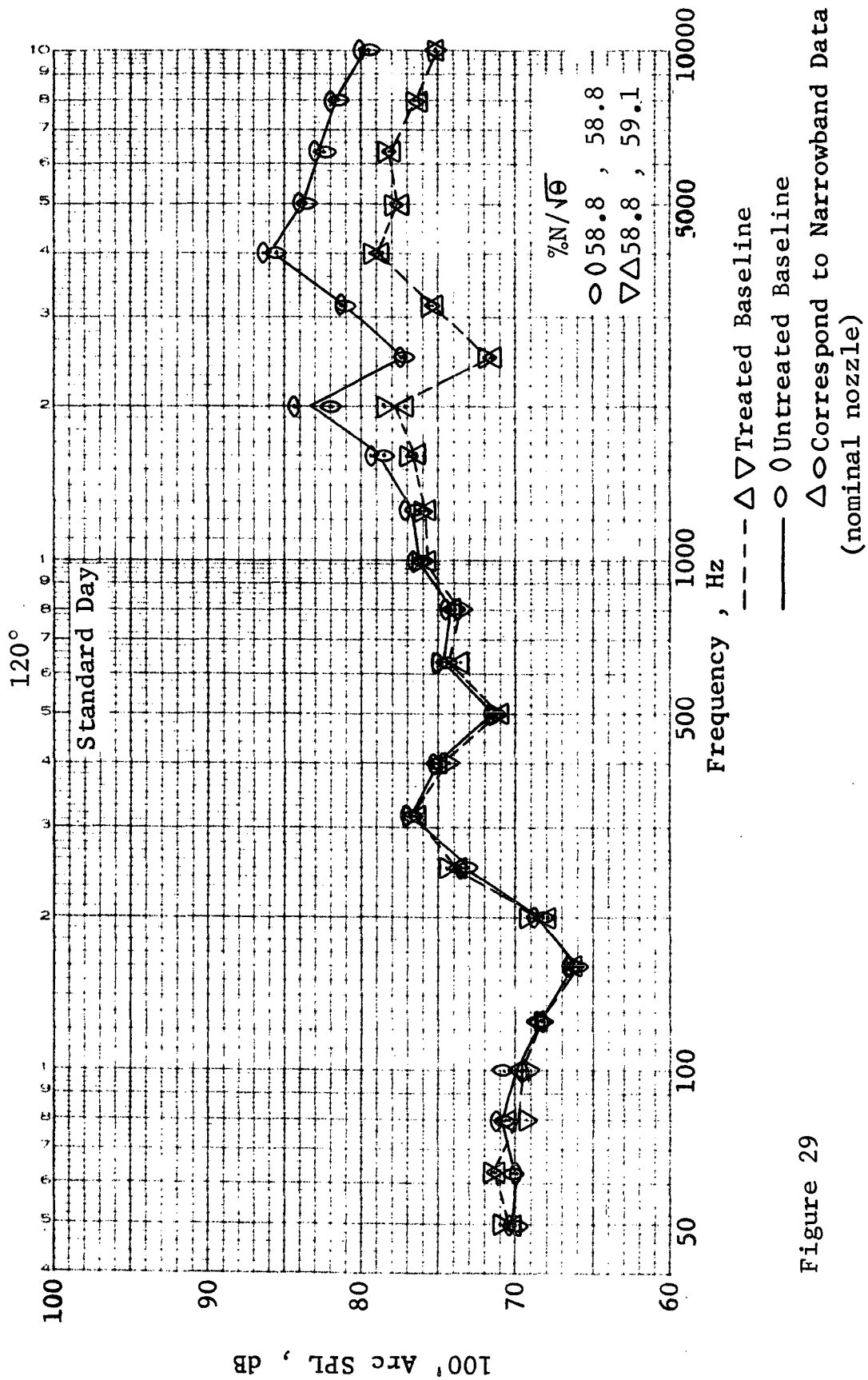


Figure 29

QEP FAN B  
 SCALE MODEL RESULTS  
 100' ARC SPL  
 TREATED VS UNTREATED  
 TAKEOFF

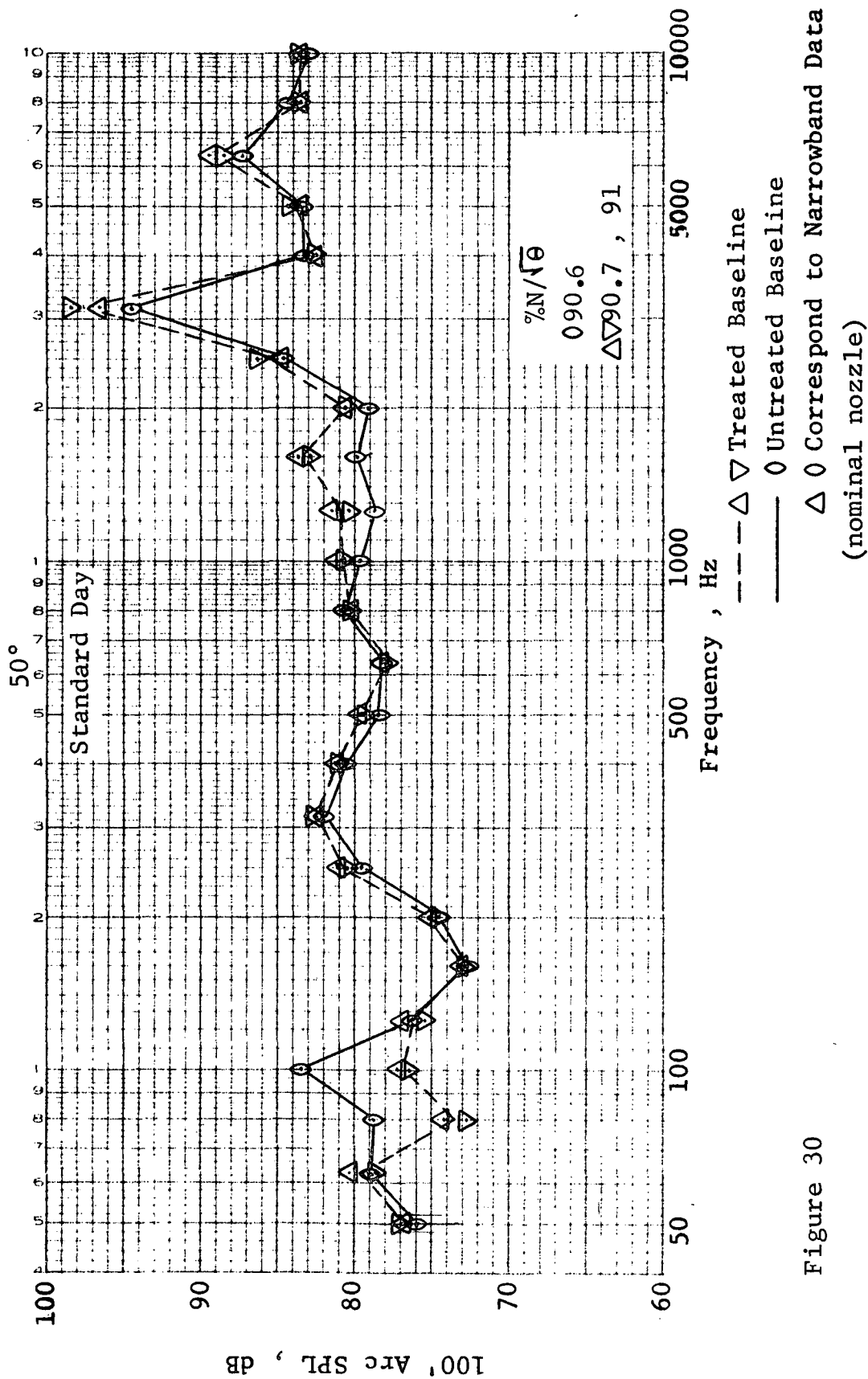


Figure 30

QEP FAN B  
 SCALE MODEL RESULTS  
 100' ARC SPL  
 TREATED VS UNTREATED  
 TAKEOFF

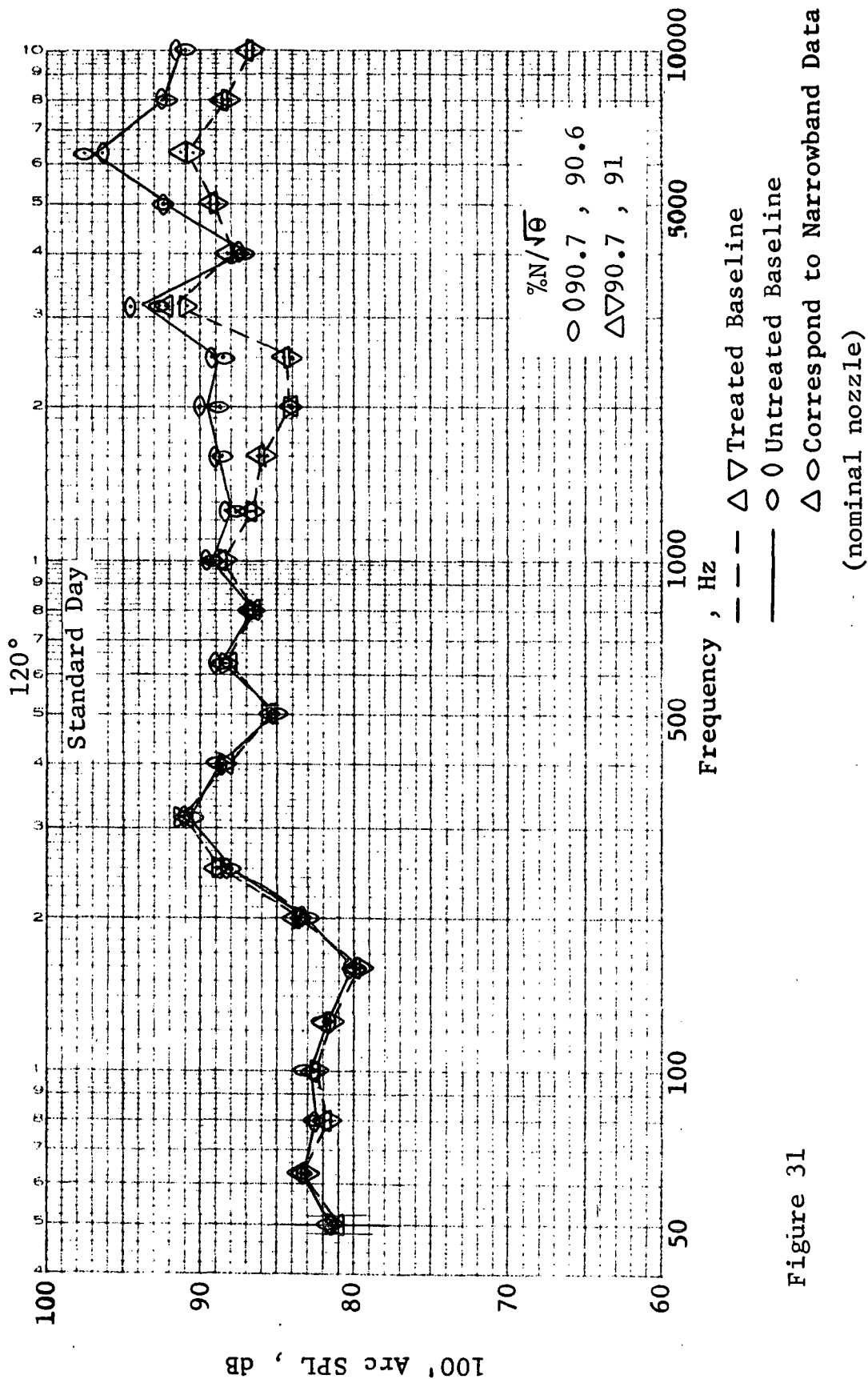


Figure 31

QEP FAN B SCALE MODEL RESULTS  
SOUND POWER LEVELS AT APPROACH  
TREATED VS UNTREATED

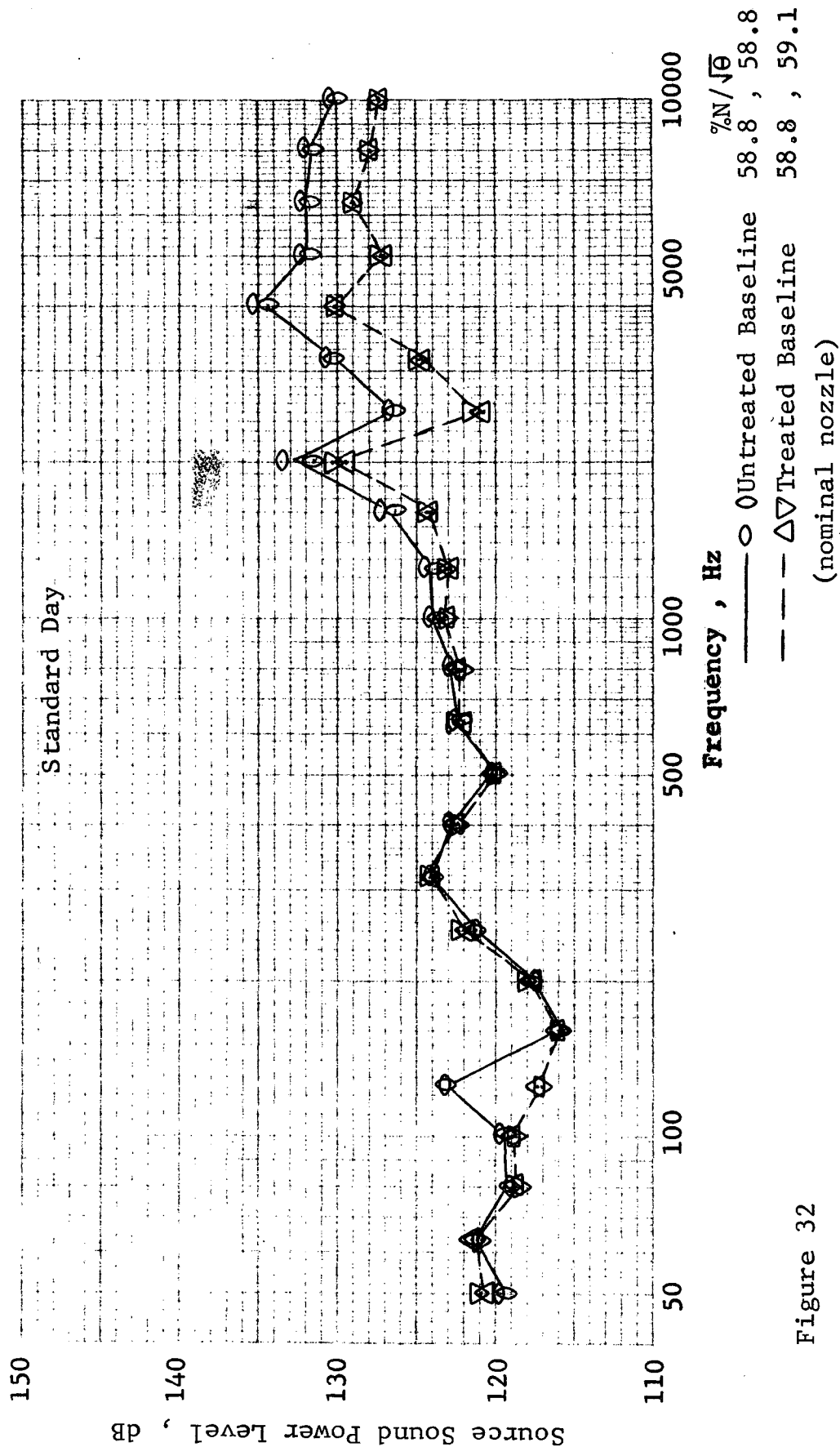


Figure 32

QEP FAN B SCALE MODEL RESULTS  
SOUND POWER LEVELS AT TAKEOFF  
TREATED VS UNTREATED

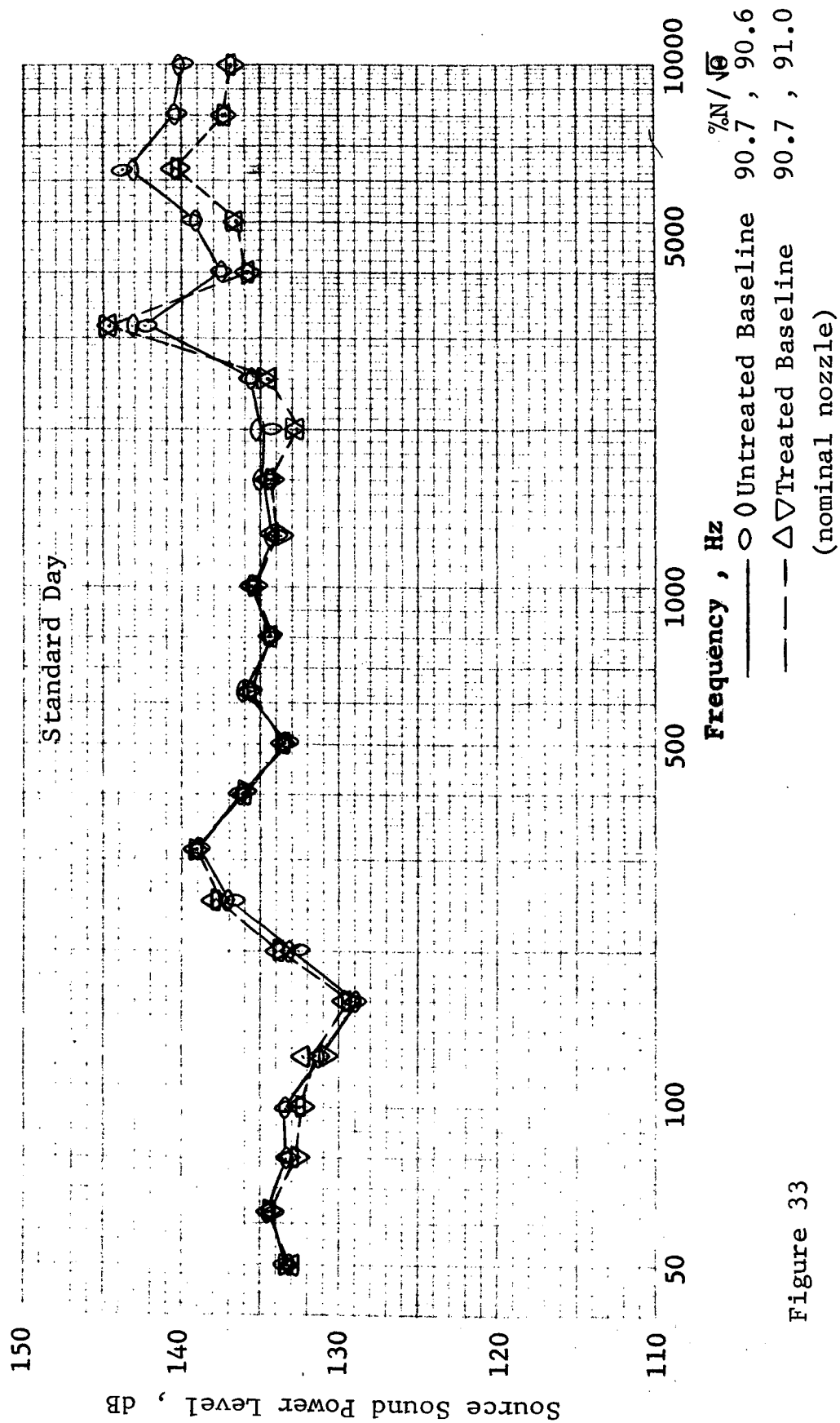


Figure 33

#### D. SCALED-UP TO FULL SCALE RESULTS

In order to obtain a picture of the full scale results, the scale model data was scaled up to full scale (see Section VI-B for details of the scaling procedure). Figures 34 - 39 present 200 foot (61.0 m) sideline perceived noise levels for both the treated and untreated configurations at approach and takeoff thrust levels for each of the three fan nozzle sizes tested. There was a definite noise reduction around the arc for all three nozzles at approach thrust due to the acoustic treatment, with noticeably greater reduction occurring in the rear quadrant. At takeoff thrust, the noise reduction was less in the aft quadrant for the three nozzles while no reduction occurred in the front quadrant for the large and small nozzle sizes. The treated fan with nominal nozzle resulted in a 3 dB increase in 200 foot (61.0 m) sideline PNL at  $40^\circ$ .

In all cases, the fan noise was aft noise dominant with the aft peak being more pronounced for the untreated case at high speed. It is also observed that the fan frame acoustic treatment as it was designed was more effective in the rear quadrant.

Figures 40 - 43 present the variation of maximum 200 foot (61.0 m) sideline PNL with corrected speed. The approach and takeoff points which have been examined in detail are shown. There has been a noise reduction over the entire speed range for each of the three nozzles.

It is interesting to note the dip in the results from the unsuppressed fan with the nominal nozzle at about 85% corrected speed. This, in part, may

account for the less than expected suppression results at takeoff thrust. The suppressed perceived noise level increased smoothly with increasing speed so that at 85% corrected speed, where the unsuppressed results decreased, the delta between the two configurations was reduced. Whereas with the large nozzle, the reduction due to the treatment was consistent over the entire speed line. Although a slight fall off was noticeable around 79% fan speed, it was not as severe as with the nominal nozzle. Likewise, the suppression varied smoothly with speed with the small nozzle, the amount of suppression gradually decreasing with increasing speed.

Another data presentation which provides more insight into the thrust maximum PNL situation is an iso-noise map. Figure 43 presents this information for the untreated case. Lines of constant maximum PNL, fan speed, and fan thrust appear along with the three operating lines. The identification of a point along a constant thrust line which produces the least noise represents an improvement from an acoustics viewpoint.

At both takeoff (100% thrust) and approach (39% thrust) points, the constant PNL lines are such that at operating points other than on the nominal operating line noise increases.

At 80% thrust, the large nozzle produces the lowest noise. Traversing the line of constant thrust, it can be seen that the noise decreases from more than 117 PNdB with the small nozzle to less than 115 PNdB with the large nozzle. However, the important approach and takeoff thrust levels do not show this trend.

The iso-noise map, Figure 44, shows basically the same result as in the untreated case. At approach static thrust, the constant thrust, speed and PNL lines are for all practical purposes parallel. At takeoff thrust, movement off the nominal nozzle increases noise. Thus, nozzle variations do not provide a means of noise reduction at these critical points.

Figure 45 shows the PNL for a level flyover of a single uninstalled fan at 370 feet (112.8 m) with a flight speed of 279 feet per second (85.0 m/sec), flight Mach number .25.

The PNL directivity shows a maximum angle noise reduction of 4.3 PNdB. Also included in Figure 45 are the maximum PNL predictions made before testing began. The suppressed level is very close to that measured while the unsuppressed level differs by about 1.7 PNdB. The suppression effectiveness was less than expected being 4.3 PNdB as opposed to a predicted level of 5.6 PNdB.

Figure 46 presents the PNL for a 1000 foot (304.8 m) level flyover of a single uninstalled fan at Mach number 0.25. At this condition, a noise increase is noted in the front, but peak PNL has been reduced 3.8 PNdB. The unsuppressed prediction is very close to that measured. However, the power suppression resulted in a 3.5 PNdB difference in the suppressed maximum.



QEP FAN B  
 FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS  
 200' SIDELINE PNL

TREATED VS UNTREATED

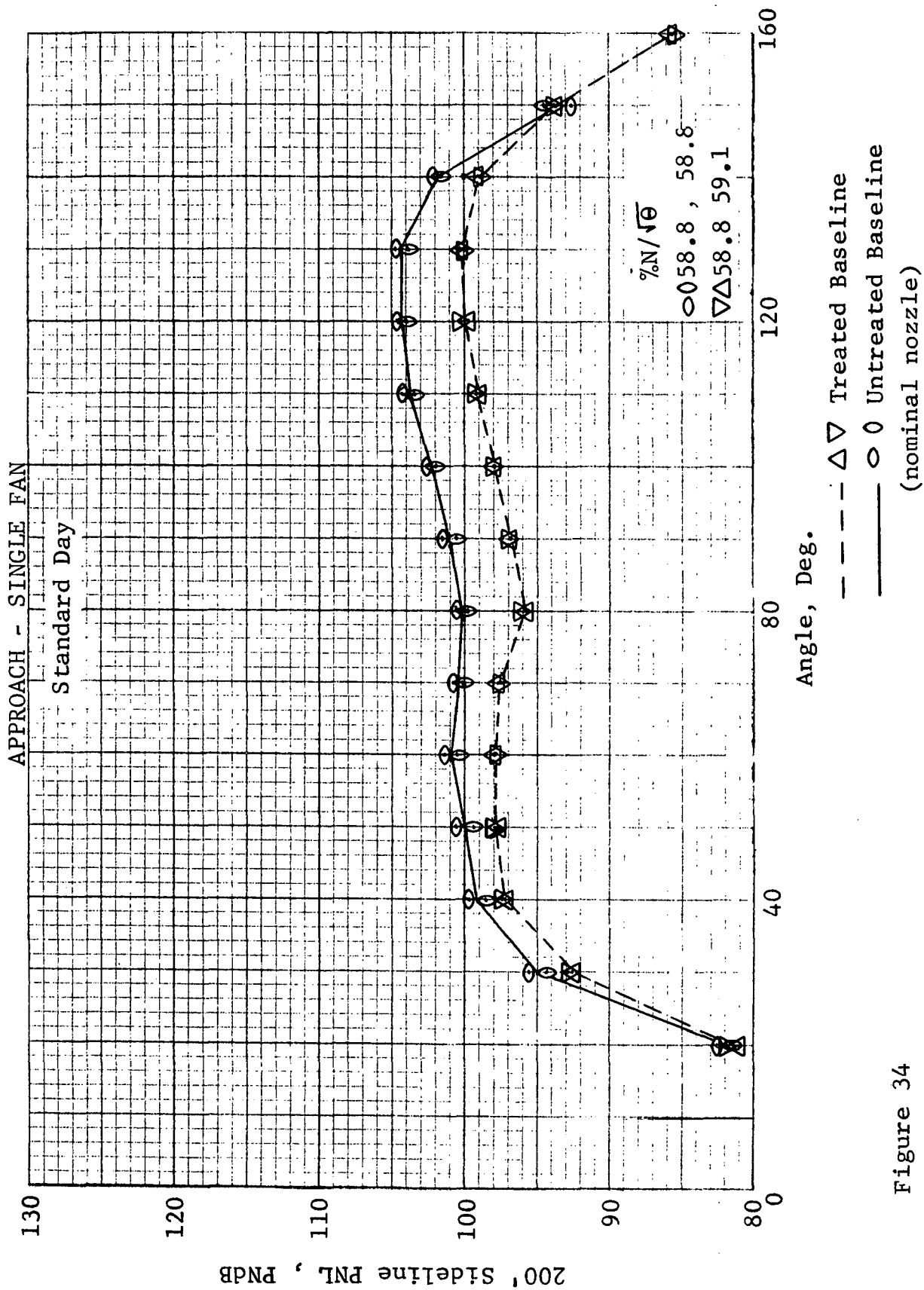


Figure 34

QEP FAN B  
 FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS  
 200' SIDELINE PNL  
 TREATED VS UNTREATED  
 TAKEOFF - SINGLE FAN

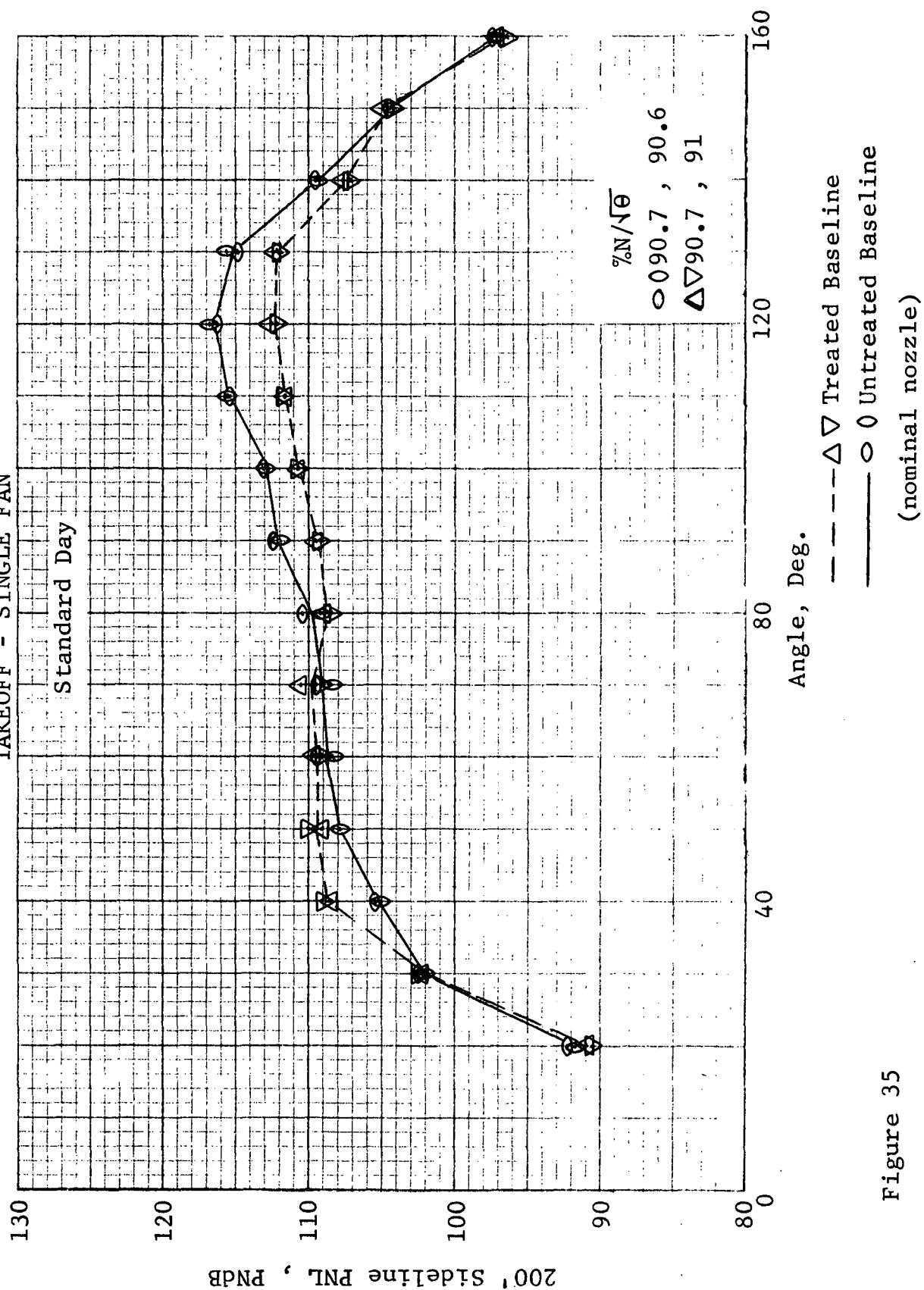


Figure 35

QEP FAN E

FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS

200' SIDELINE PNL

TREATED VS UNTREATED

APPROACH - SINGLE FAN

Standard Day

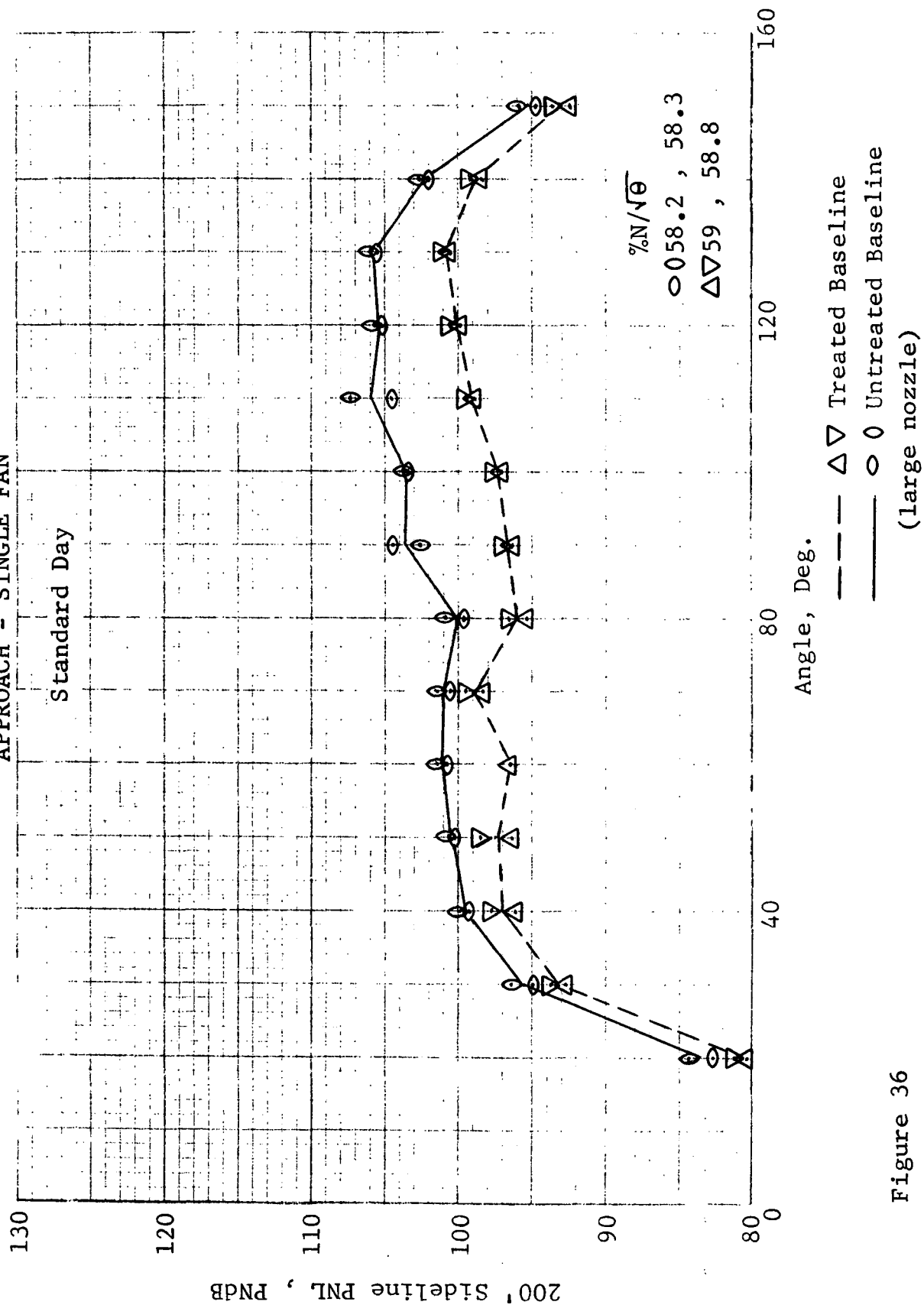


Figure 36

QEP FAN B  
 FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS  
 200' SIDELINE PNL  
 TREATED VS UNTREATED  
 TAKEOFF - SINGLE FAN

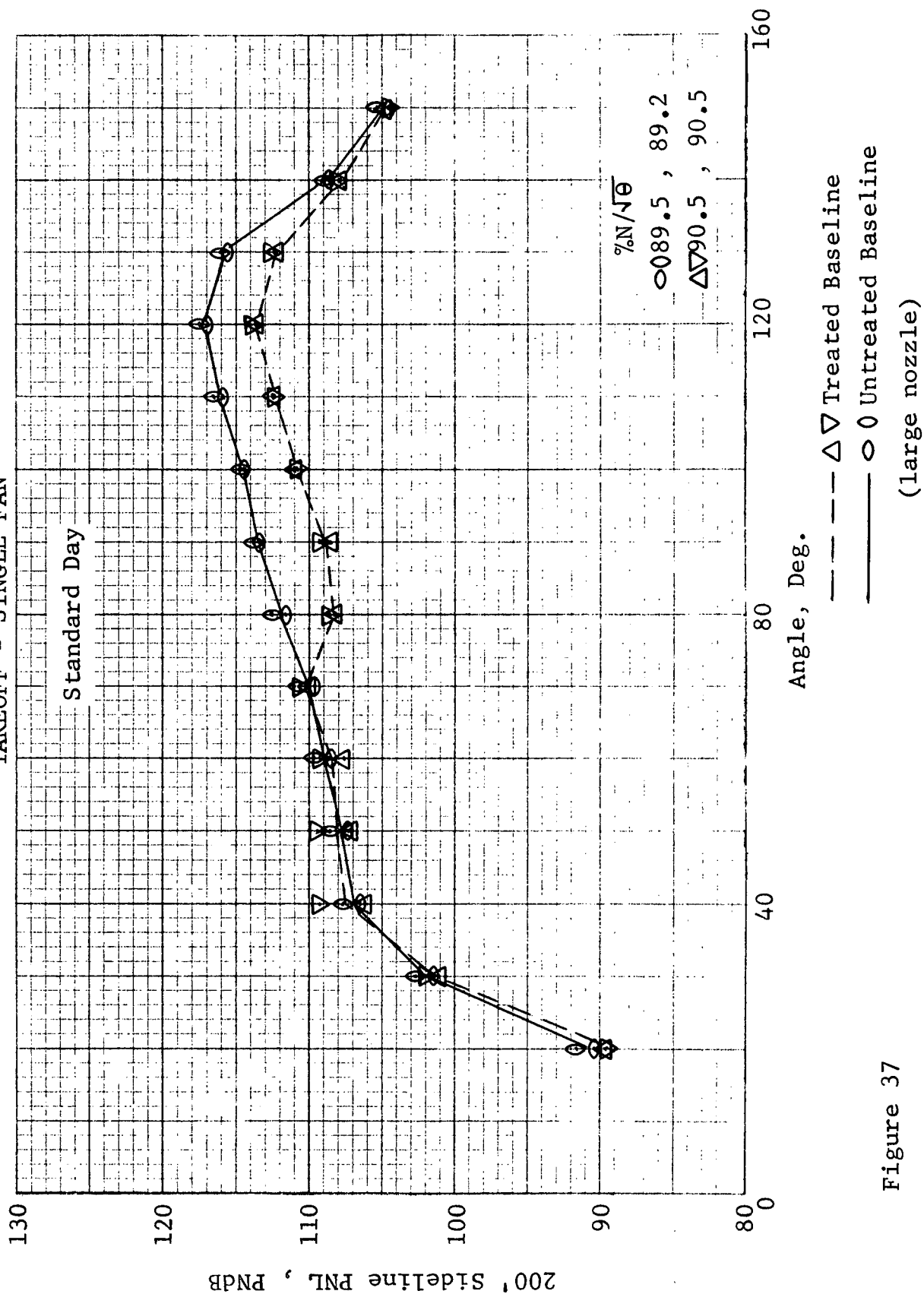


Figure 37

QEP FAN B

FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS

200' SIDELINE PNL

TREATED VS UNTREATED

APPROACH - SINGLE FAN

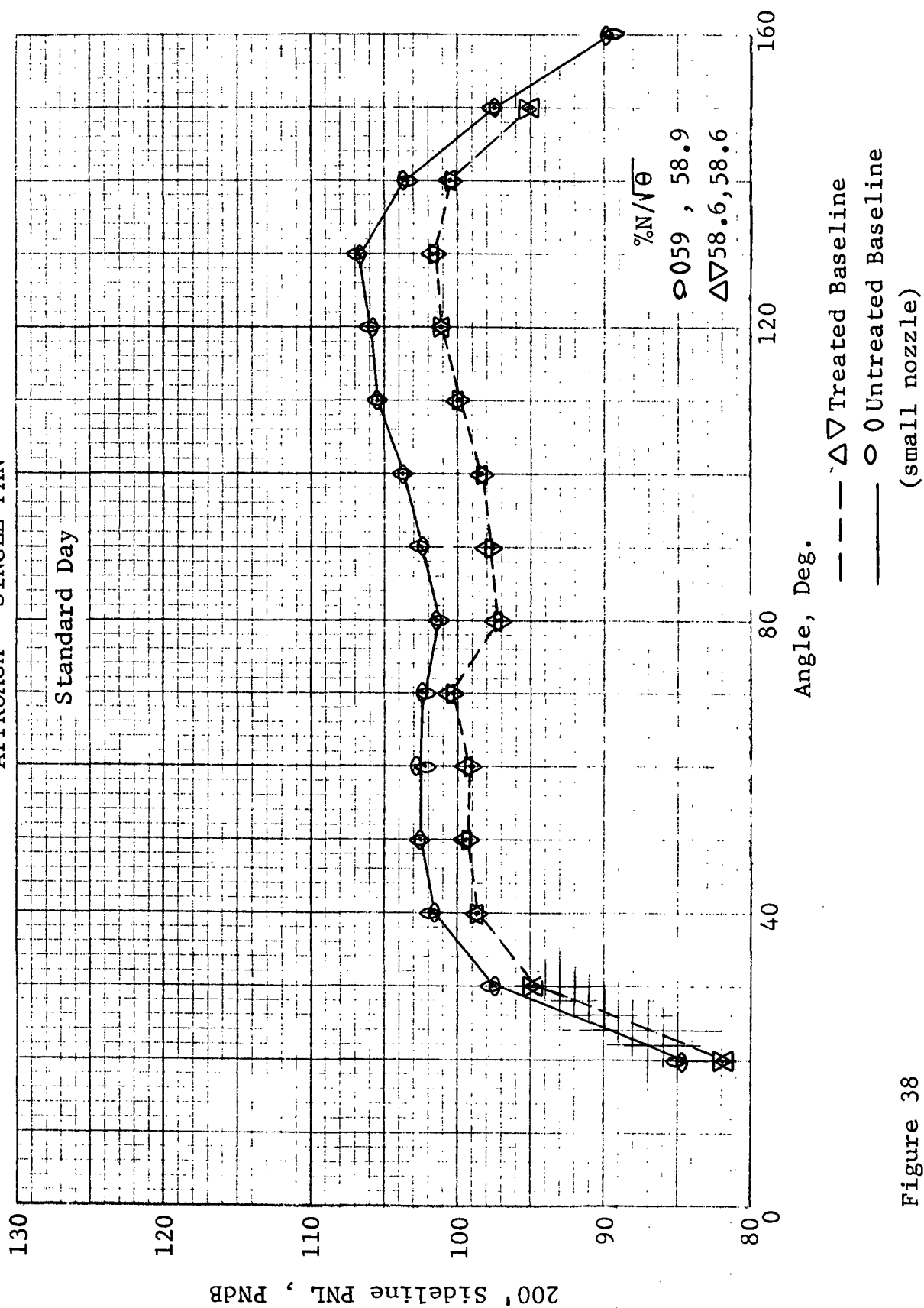


Figure 38

QEP FAN B  
 FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS  
 200' SIDELINE PNL  
 TREATED VS UNTREATED  
 TAKEOFF - SINGLE FAN

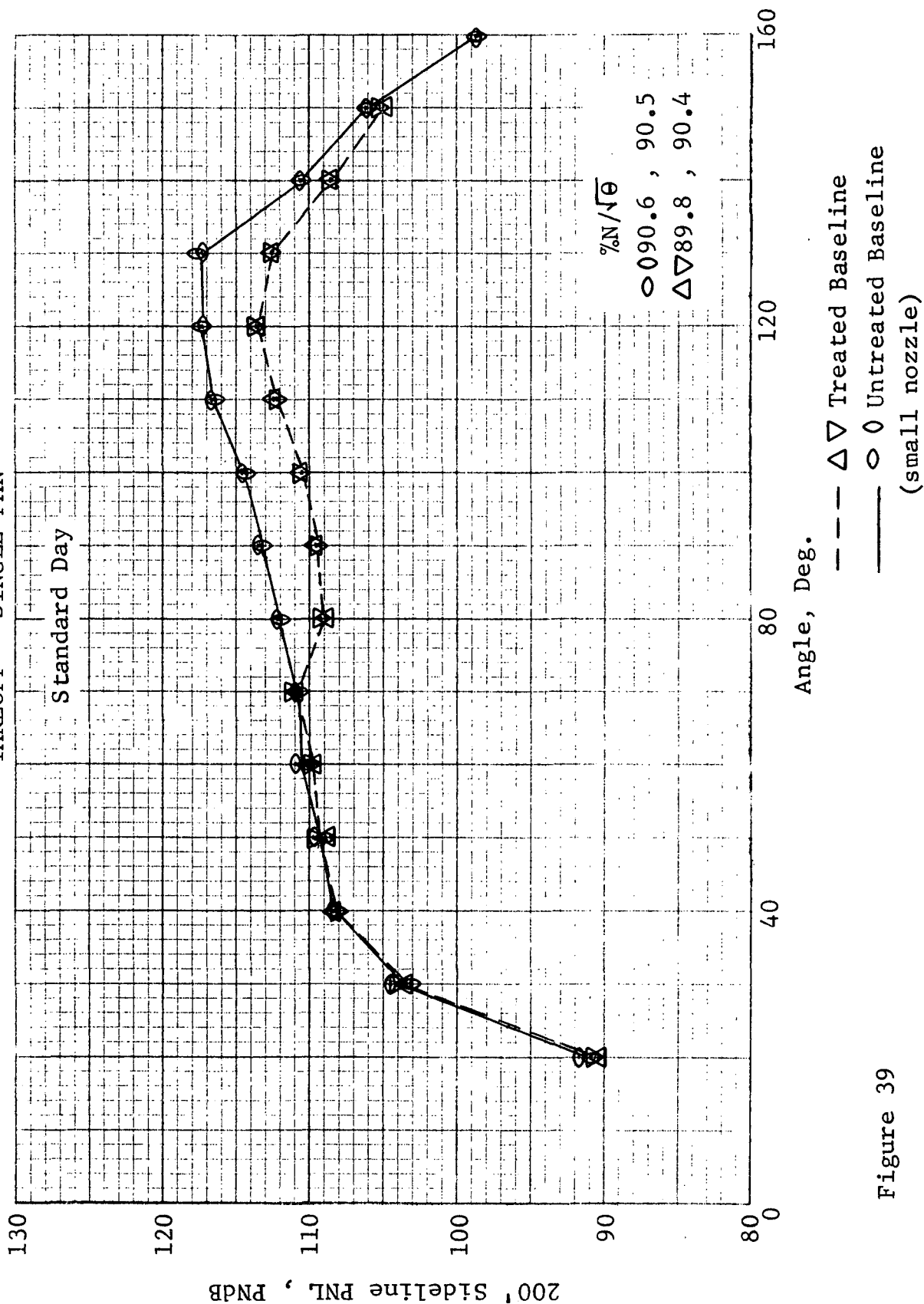
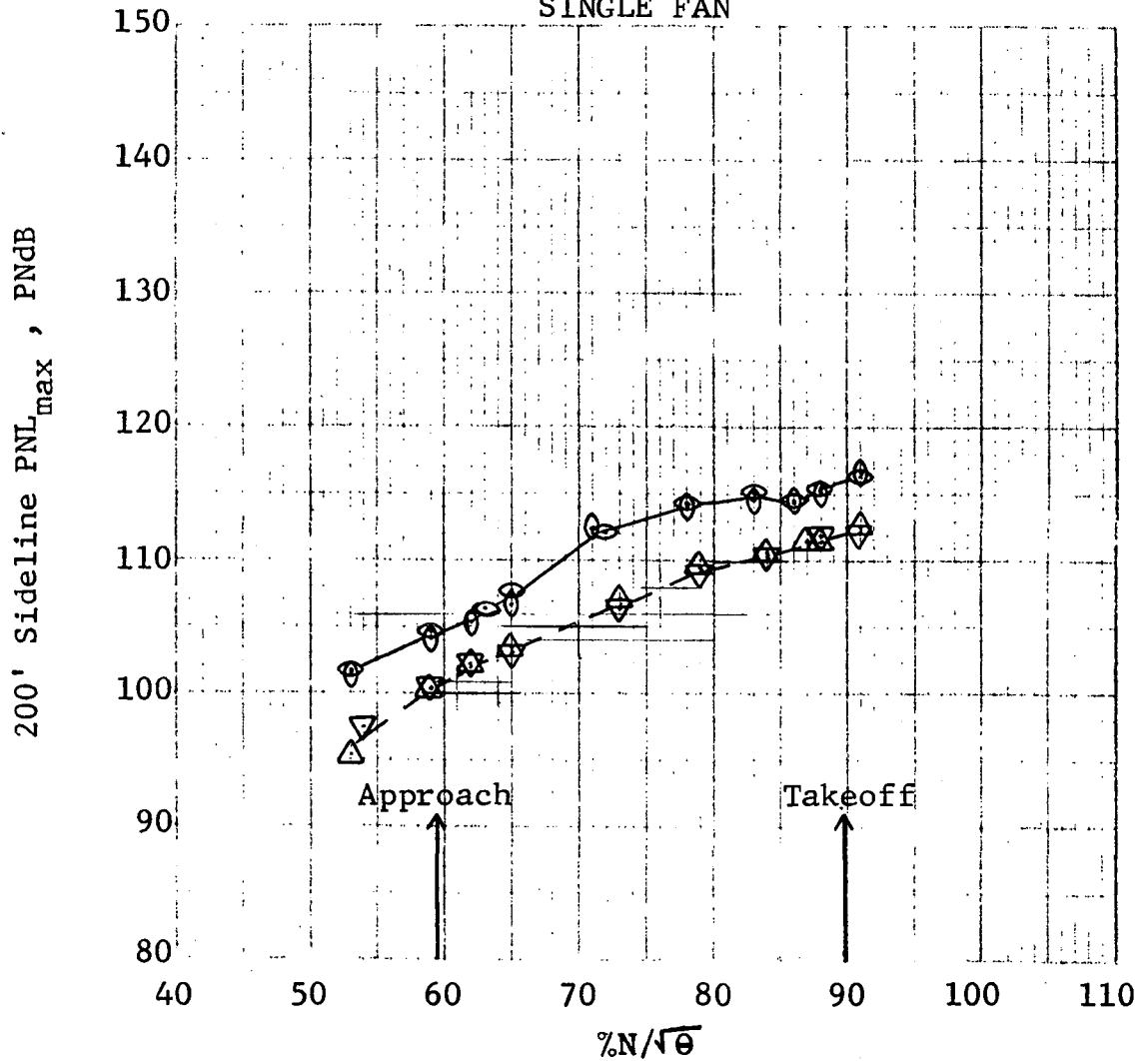


Figure 39

QEP FAN B  
 FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS  
 200' SIDELINE MAX PNL  
 TREATED VS UNTREATED  
 STANDARD DAY  
 SINGLE FAN

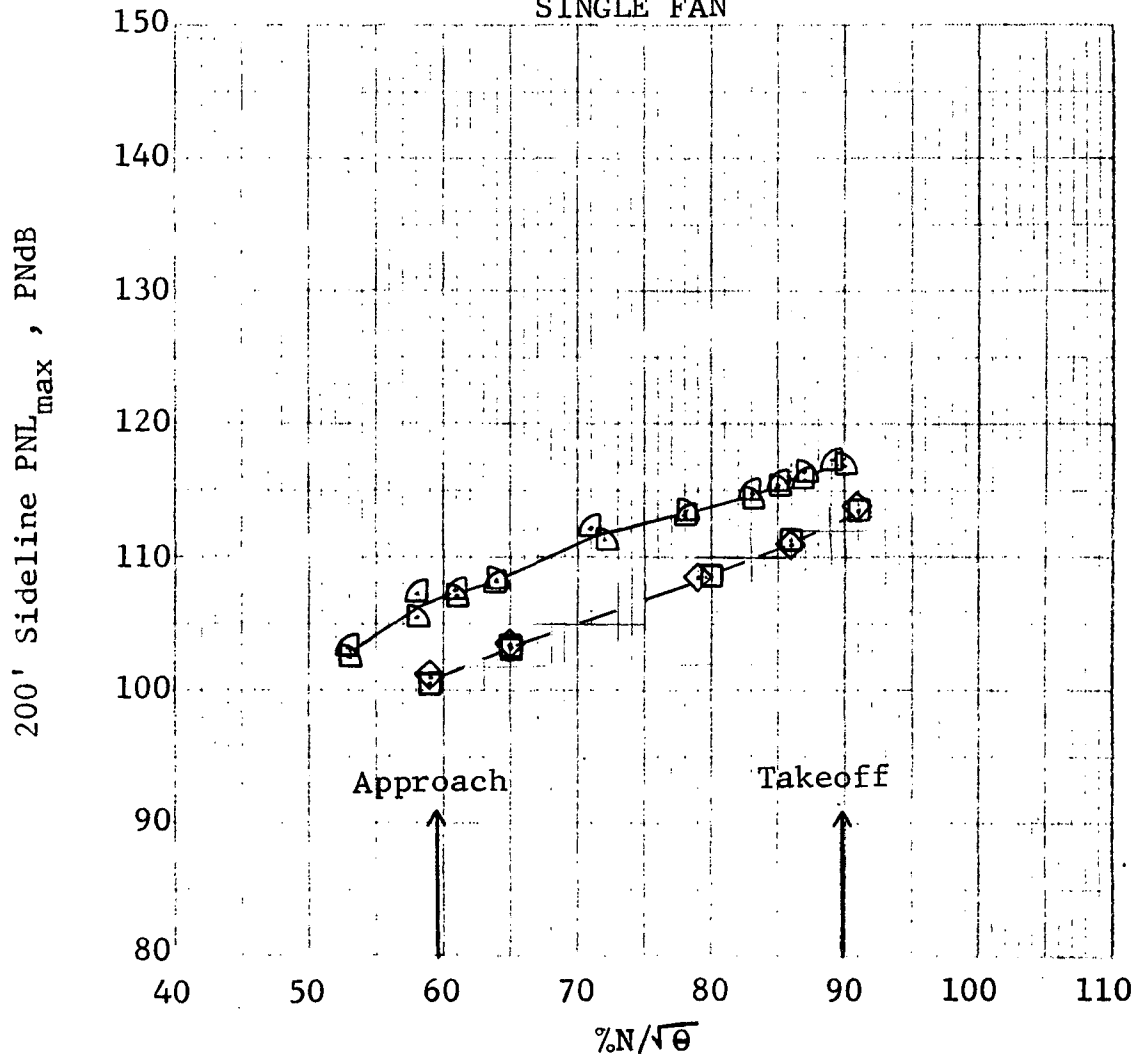


100%=3625 rpm

--- Δ ▽ Treated  
 ——— ○ ◊ Untreated  
 (nominal nozzle)

Figure 40

QEP FAN B  
 FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS  
 200' SIDELINE MAX PNL  
 TREATED VS UNTREATED  
 STANDARD DAY  
 SINGLE FAN



100%=3625 rpm

--- ◊ Treated  
 — △ Untreated  
 (large nozzle)

Figure 41



QEP FAN B  
 FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS  
 200' SIDELINE MAX PNL  
 TREATED VS UNTREATED  
 STANDARD DAY  
 SINGLE FAN

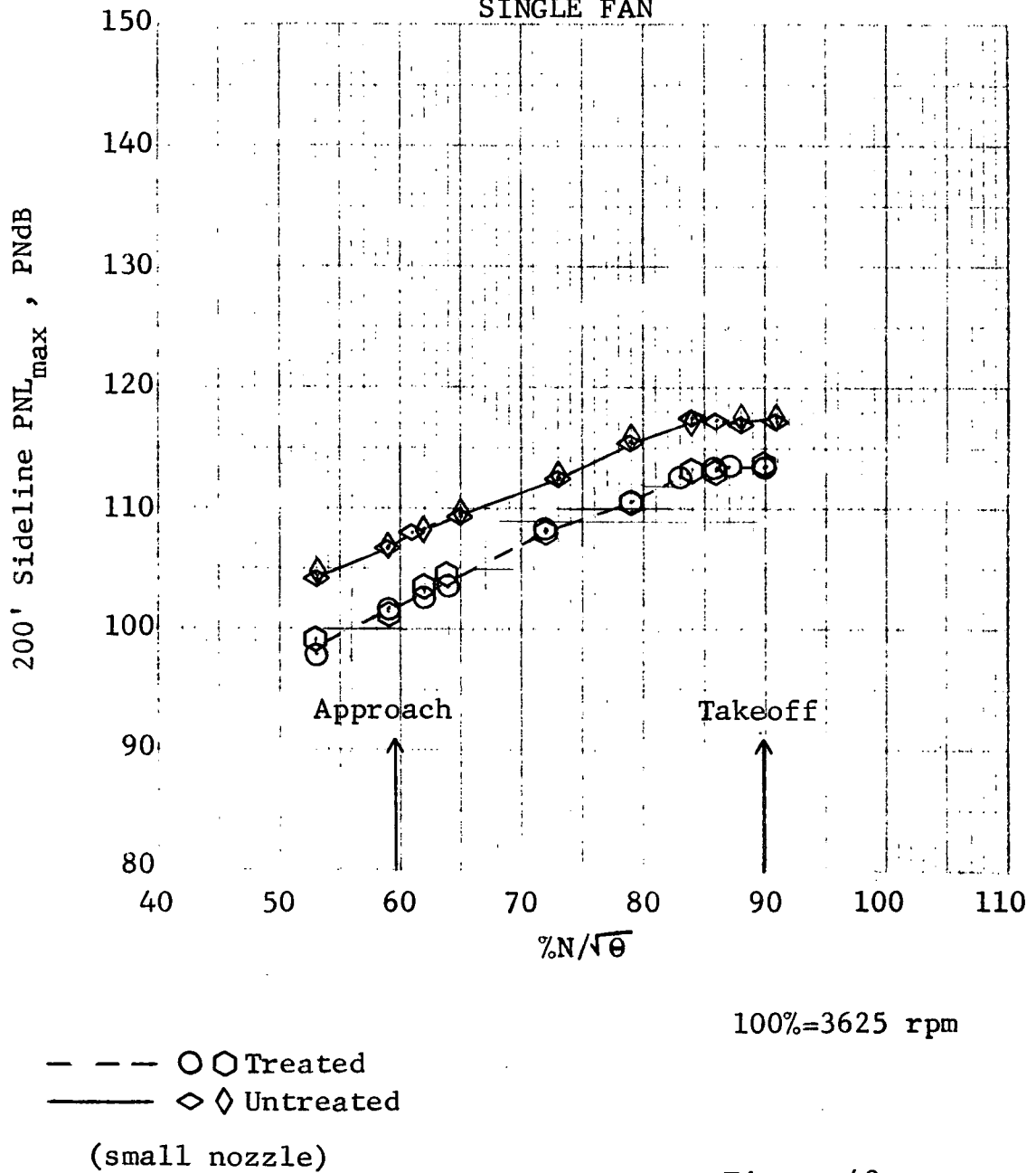


Figure 42

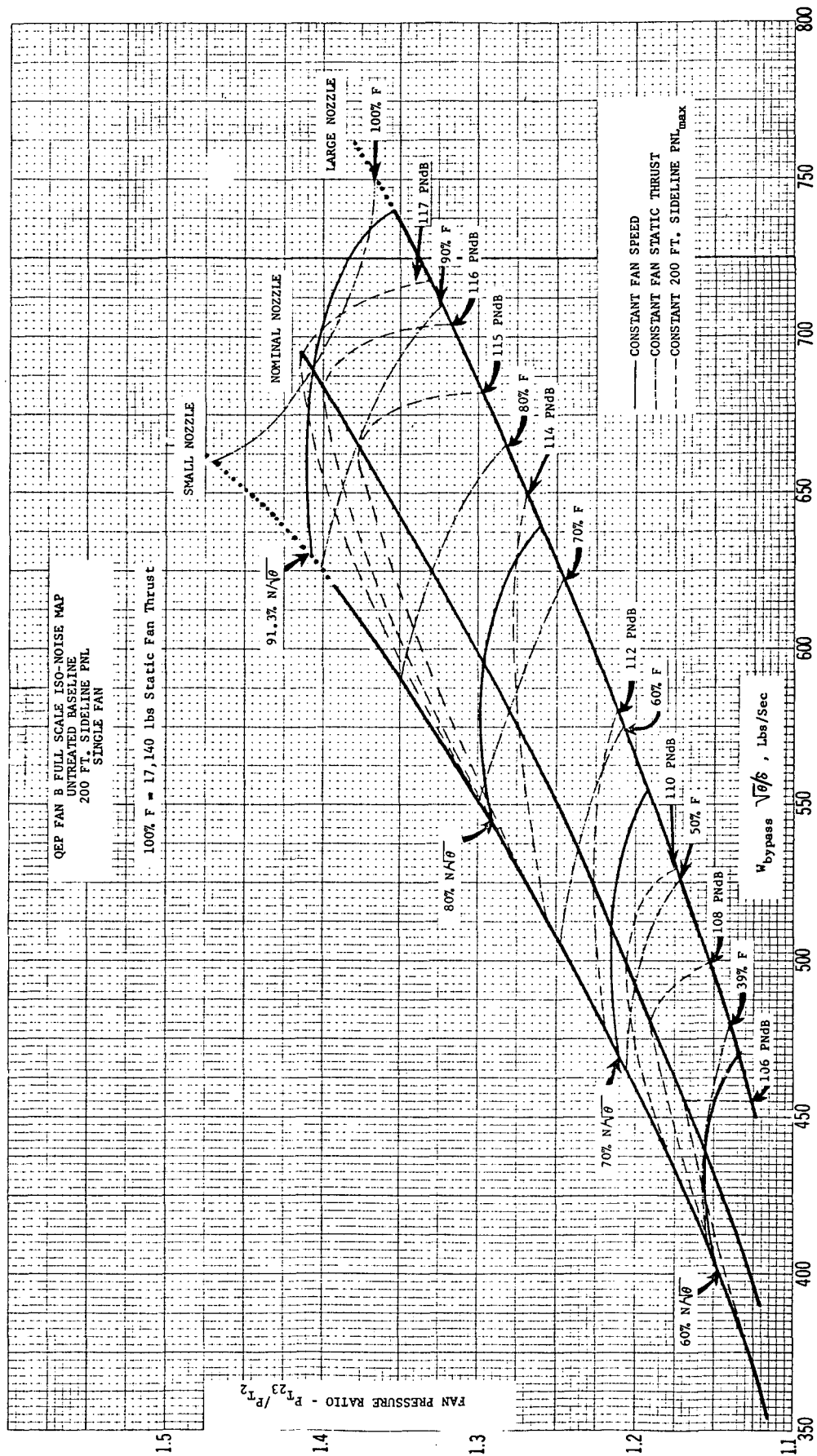


Figure 43

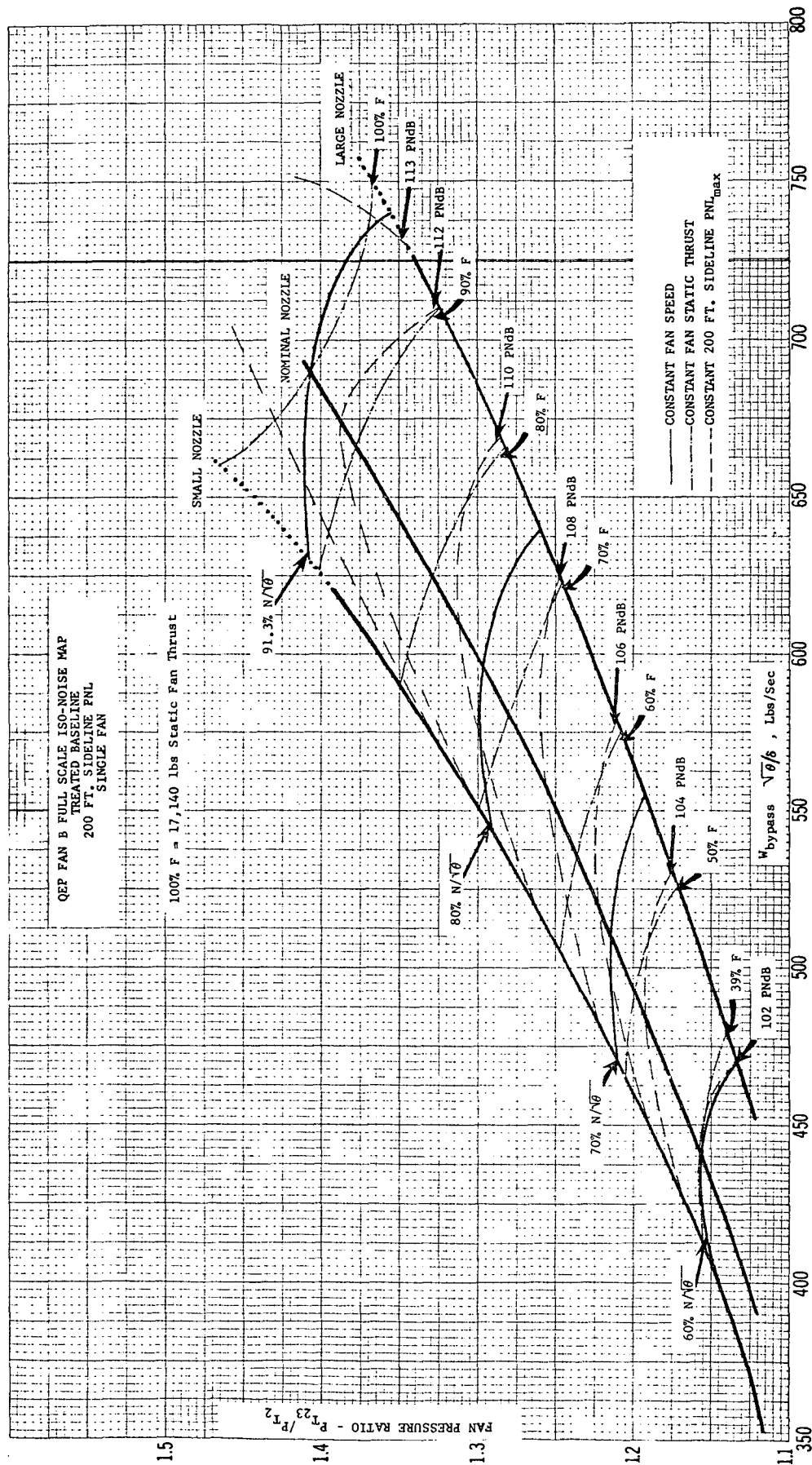
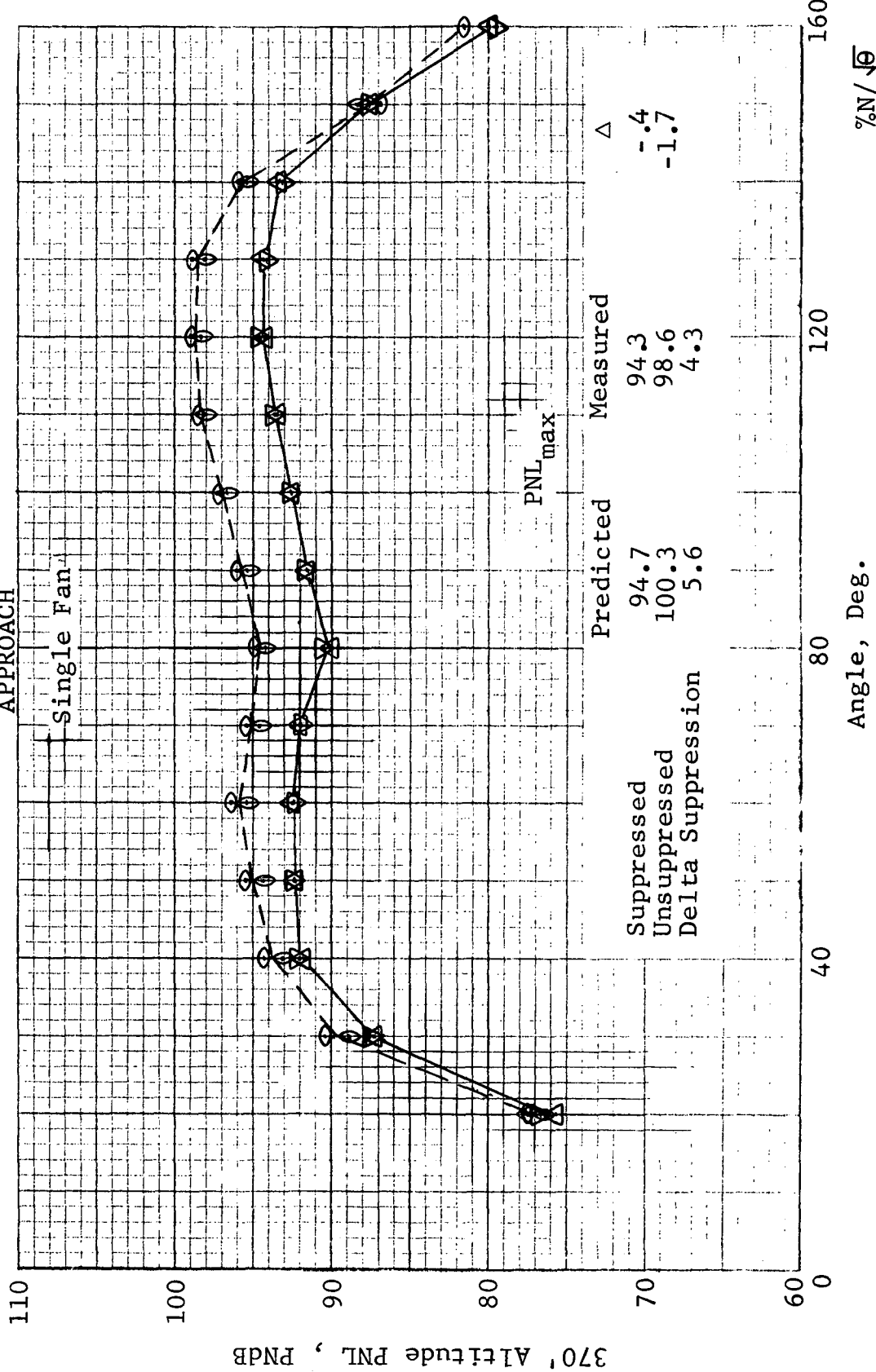


Figure 44

QEP FAN B  
 FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS  
 LEVEL FLYOVER

77°F DAY

APPROACH



$V_{plane}=279\text{Ft.}/\text{Sec.}$

Altitude=370'

Nominal Nozzle

$-- \circ$  Untreated Baseline 58.8 , 58.8  
 $-\Delta-$  Treated Baseline 58.8 , 59.1

Figure 45

## FULL SCALE PROJECTIONS FROM SCALE MODEL RESULTS

LEVEL FLYOVER

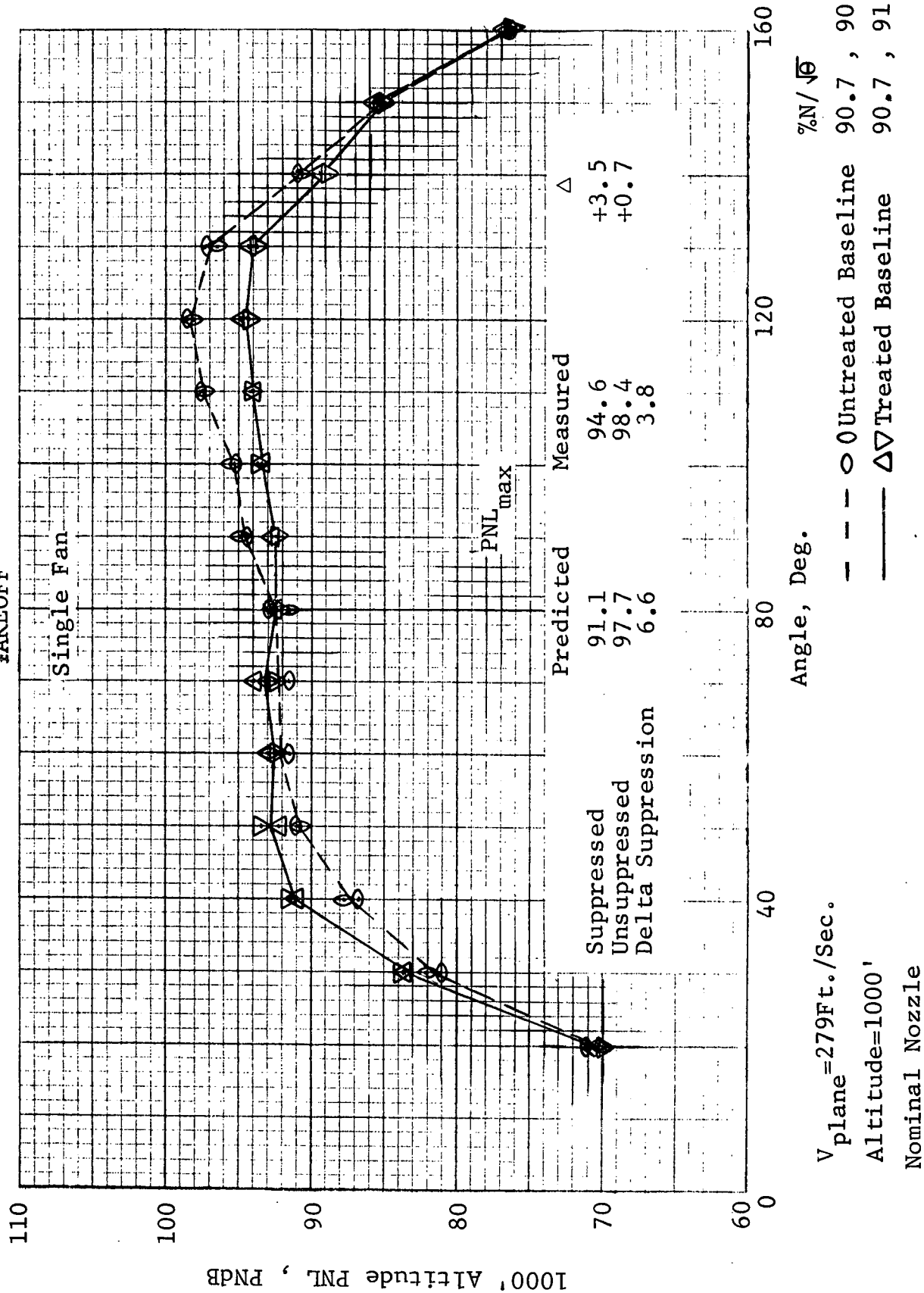
77°F DAY  
TAKEOFF

Figure 46

### VIII. CONCLUSIONS

From these data, it can be concluded:

1. On this fan exhaust nozzle area, changes did not reduce noise at takeoff and approach thrust levels; although the large nozzle (16% oversized) did show the lowest noise in the mid-thrust range.
2. Fan frame acoustic treatment was effective in reducing maximum sideline PNL. The suppression obtained was over a wide frequency range, 1 - 10 KHz.
3. Pretest flyover noise predictions agreed quite well with test results for unsuppressed noise.

Summarizing the results, projections of full scale Fan B with nominal nozzle indicate the following single fan, maximum Perceived Noise Levels (PNL) for a level flyover:

FAN B LEVEL FLYOVER PROJECTIONS  
MAXIMUM PERCEIVED NOISE LEVELS  
SINGLE FAN

	<u>Untreated</u>	<u>Treated</u>
Takeoff 1000 ft (304.8 m) altitude $M_o = .25$	98.4 PNdB	94.6 PNdB
Approach 370 ft (112.8 m) altitude $M_o = .25$	98.6 PNdB	94.3 PNdB

The 200 foot (61.0 m) sideline maximum PNL's for a single full stage Fan B were as follows:

Full Scale Fan B  
200 Foot (61.0 M) Sideline, Maximum PNL

	Approach*	Takeoff**
Nominal nozzle, untreated	104.4 PNdB	116.6 PNdB
Nominal nozzle, treated	100.2 PNdB	112.4 PNdB
Large nozzle, untreated	106.0 PNdB	117.2 PNdB
Large nozzle, treated	100.8 PNdB	113.6 PNdB
Small nozzle, untreated	106.8 PNdB	117.5 PNdB
Small nozzle, treated	101.6 PNdB	113.6 PNdB

\*6684 pounds (29,744 newtons) static thrust

\*\*17,140 pounds (76,277 newtons) static thrust

## IX. APPENDIX

Tables A1 - A24 contain the 1/3 octave scale model data used to prepare this report. The data presented is for the 100 foot (30.5 m) arc and has been corrected to Standard Day conditions. Tables A1 - A4 contain the data for the untreated configuration with nominal nozzle for speeds as close as possible to 60, 70, 80 and 90% corrected fan speed. Tables A5 - A8 present the data for the treated configuration at these speeds. Tables A9 - A16 contain the same set of information for the fan with large nozzle and Tables A17 - A24 present the data for the small nozzle.



100' (30.5M) ARC ; 58.8%  $N_{fc}$  ; NOMINAL NOZZLE ; UNTREATED

TABLE A1

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 71.9%N<sub>fc</sub> ; NOMINAL NOZZLE ; UNTREATED

PAGE 1 NASA QUIET ENGINE 1/2 SCALE FAN									
MODEL SOUND PRESSURE LEVELS PRESENTED FOR STANDARD DAY 2 ANGLES FROM INLET IN DEGREES (AND RADIANS)									
P.O.C. DATE - MONTH 10 DAY 16 HS 7.3									
FREQ.	20	30	40	50	60	70	80	90	100
RADIAL 100, FT.	20	30	40	50	60	70	80	90	100
VEHICLE (30, M) FAN	30	40	50	60	70	80	90	100	110
CONFIG FAN B	40	50	60	70	80	90	100	110	120
LOC PPG	50	60	70	80	90	100	110	120	130
DATE 8/17/70	60	70	80	90	100	110	120	130	140
RUN 3, PT: 27	70	80	90	100	110	120	130	140	150
TAKE	80	90	100	110	120	130	140	150	160
BAR 28.8 HG S10961	90	100	110	120	130	140	150	160	170
TAMB (97351, N/M2)	100	110	120	130	140	150	160	170	180
TAMB 831 DEG F	110	120	130	140	150	160	170	180	190
WET (301, DEG K)	120	130	140	150	160	170	180	190	200
WET 771 DEG K	130	140	150	160	170	180	190	200	210
HAC (298, DEG K)	140	150	160	170	180	190	200	210	220
HAC 121.24 GM/M3	150	160	170	180	190	200	210	220	230
NFA 5510, RPM	160	170	180	190	200	210	220	230	240
NFA 5510, RPM	170	180	190	200	210	220	230	240	250
NFK 5387, RPM	180	190	200	210	220	230	240	250	260
NFK 5387, RPM	190	200	210	220	230	240	250	260	270
NFD 7488, RPM	200	210	220	230	240	250	260	270	280
NFD 7488, RPM	210	220	230	240	250	260	270	280	290
NO, BLADES	220	230	240	250	260	270	280	290	300
OVERALL MEASURED	230	240	250	260	270	280	290	300	310
OVERALL CALCULATED	240	250	260	270	280	290	300	310	320
PW	250	260	270	280	290	300	310	320	330

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TABLE A2

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 77.9%N<sub>fc</sub> ; NOMINAL NOZZLE ; UNTREATED

PAGE 1 NASA QUIET ENGINE		1/2 SCALE FAN		PROC. DATE - MONTH 10 DAY 16 HR. 7.3		ANGLES FROM INLET IN DEGREES (AND RADIAN)		PWL	
MODEL SOUND PRESSURE LEVELS PRESENTED FOR STANDARD DAY		FREQ. (30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150)		FREQ. (30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150)		FREQ. (30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150)		FREQ. (30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150)	
RADIAL 100, FT.	(30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150)	30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150	30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150	30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150	30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150	30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150	30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150	30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150	30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150
VEHICLE	63	63	63	63	63	63	63	63	63
CONFIG	80	80	80	80	80	80	80	80	80
LOC	100	100	100	100	100	100	100	100	100
DATE	8/27/70	8/27/70	8/27/70	8/27/70	8/27/70	8/27/70	8/27/70	8/27/70	8/27/70
RUN	3, P1, 28	3, P1, 28	3, P1, 28	3, P1, 28	3, P1, 28	3, P1, 28	3, P1, 28	3, P1, 28	3, P1, 28
TAPE	28.8 HQ S1096	28.8 HQ S1096	28.8 HQ S1096	28.8 HQ S1096	28.8 HQ S1096	28.8 HQ S1096	28.8 HQ S1096	28.8 HQ S1096	28.8 HQ S1096
BAR	315	315	315	315	315	315	315	315	315
TAB	84	84	84	84	84	84	84	84	84
THET	771	771	771	771	771	771	771	771	771
MACT	20.94	20.94	20.94	20.94	20.94	20.94	20.94	20.94	20.94
NFA	5970	5970	5970	5970	5970	5970	5970	5970	5970
NFK	5811	5811	5811	5811	5811	5811	5811	5811	5811
NFD	7488	7488	7488	7488	7488	7488	7488	7488	7488
NO, BLADES	26	26	26	26	26	26	26	26	26
OVERALL MEASURED		OVERALL MEASURED		OVERALL MEASURED		OVERALL MEASURED		OVERALL MEASURED	
OVERALL CALCULATED		OVERALL CALCULATED		OVERALL CALCULATED		OVERALL CALCULATED		OVERALL CALCULATED	
PND8		PND8		PND8		PND8		PND8	

TABLE A3



QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 58.8%N<sub>FC</sub> ; NOMINAL NOZZLE ; TREATED

PAGE 1 NASAQUIETENGINE		1/2SCALEFAN		PROC. DATE - MONTH 12 DAY 8 HR. 20.8											
MODEL	FREQ.	SOUND PRESSURE LEVELS	PRESENTED FOR STANDARD DAY	90	100	110	120	130	140	150	160				
RADIAL 100, FT. (30, M)	50	72.3	67.9	69.5	69.8	68.0	66.4	69.6	69.7	70.3	70.1	70.9	72.8		
VEHICLE	63	64.9	65.3	65.3	68.6	67.7	65.4	75.7	68.5	69.4	71.3	70.7	74.7		
CONFIG	80	61.3	63.6	63.8	66.0	66.2	65.4	67.0	68.6	69.6	70.4	71.6	76.3		
LOC PTO	100	64.5	67.1	70.8	67.3	66.9	65.6	67.7	67.7	68.7	69.8	71.9	71.9		
DATE 10/6/70	125	65.0	66.0	64.7	66.9	66.7	66.3	66.5	66.5	67.3	68.5	70.3	71.9		
RUN 17, PT. 202	160	63.7	62.9	64.5	64.1	66.2	63.9	66.0	64.9	66.0	66.2	67.4	68.5		
TAPE 19543	200	62.7	61.6	65.4	62.6	64.5	63.3	66.9	65.4	67.7	67.9	69.9	72.7		
BAR 29.0 HG	250	65.0	65.7	65.6	67.2	66.9	68.7	70.5	71.4	72.6	73.7	75.0	75.3		
TAMB (97760, N/M2)	315	66.3	67.7	68.7	69.5	69.4	70.2	70.2	72.7	73.8	75.3	77.4	77.5		
TAMB (295, DEG K)	400	67.9	70.9	69.9	70.2	70.3	70.1	71.6	69.4	73.7	74.9	75.1	74.6		
TNET (60, DEG F)	500	69.7	71.0	69.9	69.4	69.4	68.2	68.4	69.4	72.9	73.8	74.8	71.9		
HACT (289, DEG K)	630	67.6	68.8	69.1	71.8	68.7	68.4	70.3	71.4	72.9	73.3	74.5	72.7		
HACT 9.52 G/M3	800	71.1	70.6	70.7	71.3	70.4	70.1	72.3	72.4	72.6	74.0	73.5	73.0		
(.00952 KG/M3)	1000	67.5	68.7	71.7	70.5	69.8	68.5	70.0	72.2	73.3	75.7	75.1	73.0		
NFA 4460, RPM	1250	70.4	71.7	71.7	71.0	70.0	69.4	69.7	70.5	72.6	76.4	76.9	74.6		
(467, RAD/SEC)	1500	82.1	80.3	80.2	76.7	76.2	74.9	75.9	76.3	78.6	77.1	78.2	81.5		
NFK 4401, RPM	2000	66.7	67.1	68.3	66.5	65.2	66.0	66.0	68.0	70.2	71.6	72.2	80.3		
(451, RAD/SEC)	2500	64.0	74.9	72.9	72.0	71.0	70.4	70.3	71.3	73.2	75.0	75.9	74.4		
NPD 7488, RPM	3000	69.9	80.8	82.7	79.9	78.5	77.4	74.9	76.5	79.4	79.8	80.8	81.6		
(784, RAD/SEC)	3500	70.6	75.3	76.7	75.2	72.3	69.7	72.3	74.2	75.7	77.5	80.0	80.7		
NO, BLADES 26	4000	78.6	79.1	77.8	76.7	74.6	72.3	72.4	73.6	75.1	78.0	80.6	82.5		
	4500	66.2	76.9	78.4	77.1	75.6	73.4	71.6	72.4	74.7	76.3	78.1	78.6		
	5000	66.5	75.8	77.7	77.0	74.7	73.5	69.2	70.2	72.3	75.0	75.4	76.4		
	5500	66.1	73.2	75.6	74.2	72.7	71.7	66.6	68.3	69.9	71.4	70.7	72.8		
	6000	67.9	73.3	73.3	70.9	68.7	65.7	64.4	64.6	66.2	67.9	66.0	68.1		
	6500	67.9	71.9	69.7	68.9	69.0	65.2	63.4	63.1	66.5	67.2	63.6	67.0		
	7000	83.8	90.0	86.9	87.0	86.2	84.5	85.3	85.3	88.6	89.8	91.0	90.7		
OVERALL MEASURED		83.8	88.2	86.9	86.3	85.5	83.5	85.3	85.3	86.0	87.5	88.6	88.0		
OVERALL CALCULATED		97.1	114.3	102.9	101.2	99.1	96.5	98.0	97.3	100.9	101.9	103.6	103.4		
PND8		97.1	114.3	102.9	101.2	99.1	96.5	98.0	97.3	100.9	101.9	103.6	103.4		

TABLE A5

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 73.0%N<sub>fc</sub> ; NOMINAL NOZZLE ; TREATED

PAGE 1 NASQUIT ENGINE		1/25 SCALE FAN SOUND PRESSURE LEVELS PRESENTED FOR STANDARD DAY - ANGLES FROM INLET IN DEGREES (AND RADIANS)															PROC. DATE - MONTH 12 DAY 8 HR. 20.9	
MODEL	FREQ.	20	30	40	50	60	70	80	90	100	110	120	130	140	150	160	P.W.L	
RADIAL 100, FT.	50	74.9	72.6	71.9	71.1	70.1	69.1	68.1	67.1	66.1	65.1	64.1	63.1	62.1	61.1	60.1	126.6	
VEHICLE (30, M)	63	68.9	67.7	67.0	66.1	65.1	64.1	63.1	62.1	61.1	60.1	59.1	58.1	57.1	56.1	55.1	127.1	
CONFIG FANB	80	65.9	64.5	63.6	62.6	61.6	60.6	59.6	58.6	57.6	56.6	55.6	54.6	53.6	52.6	51.6	125.4	
LOC PTO	100	74.9	71.2	70.4	69.4	68.4	67.4	66.4	65.4	64.4	63.4	62.4	61.4	60.4	59.4	58.4	127.2	
DATE 10/6/70	125	68.9	67.7	67.0	66.1	65.1	64.1	63.1	62.1	61.1	60.1	59.1	58.1	57.1	56.1	55.1	123.1	
RUN 17 PT. 265	200	68.2	66.5	65.6	64.6	63.6	62.6	61.6	60.6	59.6	58.6	57.6	56.6	55.6	54.6	53.6	122.3	
TAPE 19889	250	69.0	67.3	66.4	65.4	64.4	63.4	62.4	61.4	60.4	59.4	58.4	57.4	56.4	55.4	54.4	127.5	
BAR 29.0 HG	325	72.6	70.8	69.9	68.9	67.9	66.9	65.9	64.9	63.9	62.9	61.9	60.9	59.9	58.9	57.9	129.8	
(97760 N/M2)	400	74.0	72.0	71.0	70.0	69.0	68.0	67.0	66.0	65.0	64.0	63.0	62.0	61.0	60.0	59.0	131.3	
FANB 59 DEG F	500	73.2	71.5	70.6	69.6	68.6	67.6	66.6	65.6	64.6	63.6	62.6	61.6	60.6	59.6	58.6	126.8	
(294 DEG K)	630	74.9	73.9	73.0	72.0	71.0	70.0	69.0	68.0	67.0	66.0	65.0	64.0	63.0	62.0	61.0	129.1	
THET 59 DEG K	800	74.6	73.5	72.5	71.5	70.5	69.5	68.5	67.5	66.5	65.5	64.5	63.5	62.5	61.5	60.5	123.5	
(288 DEG K)	1000	73.3	72.2	71.2	70.2	69.2	68.2	67.2	66.2	65.2	64.2	63.2	62.2	61.2	60.2	59.2	128.7	
HADY 9.93 G/M3	1250	72.6	71.2	70.2	69.2	68.2	67.2	66.2	65.2	64.2	63.2	62.2	61.2	60.2	59.2	58.2	129.2	
(.00993 KG/M3)	1500	74.2	73.3	72.3	71.3	70.3	69.3	68.3	67.3	66.3	65.3	64.3	63.3	62.3	61.3	60.3	129.7	
NFA 5524 RPM	2000	73.7	72.7	71.7	70.7	69.7	68.7	67.7	66.7	65.7	64.7	63.7	62.7	61.7	60.7	59.7	129.2	
(.578 RAD/SEC)	2500	79.1	78.4	77.4	76.4	75.4	74.4	73.4	72.4	71.4	70.4	69.4	68.4	67.4	66.4	65.4	134.0	
NFK 5469 RPM	3150	69.2	68.4	67.4	66.4	65.4	64.4	63.4	62.4	61.4	60.4	59.4	58.4	57.4	56.4	55.4	130.8	
(.573 RAD/SEC)	4000	71.5	70.0	69.0	68.0	67.0	66.0	65.0	64.0	63.0	62.0	61.0	60.0	59.0	58.0	57.0	132.2	
NFD 7488 RPM	5000	77.4	76.7	75.7	74.7	73.7	72.7	71.7	70.7	69.7	68.7	67.7	66.7	65.7	64.7	63.7	135.3	
(.788 RAD/SEC)	6300	73.6	72.6	71.6	70.6	69.6	68.6	67.6	66.6	65.6	64.6	63.6	62.6	61.6	60.6	59.6	134.1	
NO. BLADES 26	8000	73.6	72.6	71.6	70.6	69.6	68.6	67.6	66.6	65.6	64.6	63.6	62.6	61.6	60.6	59.6	133.3	
	10000	71.4	70.7	69.7	68.7	67.7	66.7	65.7	64.7	63.7	62.7	61.7	60.7	59.7	58.7	57.7	134.2	
	12500	70.4	69.7	68.7	67.7	66.7	65.7	64.7	63.7	62.7	61.7	60.7	59.7	58.7	57.7	56.7	134.2	
	16000	66.2	65.6	64.6	63.6	62.6	61.6	60.6	59.6	58.6	57.6	56.6	55.6	54.6	53.6	52.6	128.7	
	20000	66.7	65.6	64.6	63.6	62.6	61.6	60.6	59.6	58.6	57.6	56.6	55.6	54.6	53.6	52.6	128.7	
OVERALL MEASURED	89.1	94.7	94.9	94.2	93.0	91.9	91.2	90.1	89.1	88.1	87.1	86.1	85.1	84.1	83.1	82.1	144.8	
OVERALL CALCULATED	87.1	93.3	93.6	93.0	91.9	91.2	90.1	89.1	88.1	87.1	86.1	85.1	84.1	83.1	82.1	81.1		
PADB 100.6	107.6	107.1	107.1	106.4	105.2	104.1	102.8	101.4	100.4	100.4	100.4	100.4	100.4	100.4	100.4	100.4		

TABLE A6

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 79.3%N<sub>fc</sub> ; NOMINAL NOZZLE ; TREAT<sub>2</sub>

PAGE 1 NASAQUIETENGINE		PROC. DATE -- MONTH 12 DAY 8 HR. 20.9															
MODEL		SOUND PRESSURE LEVELS PRESENTED FOR STANDARD DAY - ANGLES FROM INLET IN DEGREES (AND RADIAN)															
FREQ.		30	40	50	60	70	80	90	100	110	120	130	140	150	160	PWL	
RADIAL 100' FT.	50	76.2	74.8	74.1	73.8	73.6	73.8	76.1	76.8	77.8	78.1	79.0	82.5	86.2	89.5	129.5	
VEHICLE 15FAN	63	70.5	72.2	73.2	74.3	75.1	76.0	78.9	77.5	78.7	79.1	79.9	83.1	86.1	89.3	129.8	
CONFIG FANB	80	67.5	69.9	70.7	72.0	73.1	74.0	78.9	77.5	78.7	79.1	79.9	83.1	86.1	89.3	128.4	
LOC PTO	100	73.8	72.1	75.9	77.4	76.6	78.4	79.2	78.6	77.8	78.5	79.3	82.3	84.7	86.9	131.3	
DATE 10/6/70	125	71.4	72.5	73.1	73.4	73.1	73.6	74.4	75.3	76.5	77.8	78.3	79.6	81.0	80.1	128.2	
RUN 17 PT. 266	150	70.4	70.7	70.3	71.2	70.3	71.0	71.8	72.6	73.5	74.5	75.4	77.2	78.9	81.5	129.1	
TAPE 19889	200	75.7	72.8	71.3	72.0	71.0	72.8	75.2	76.0	76.9	77.7	79.4	82.0	84.0	86.6	132.6	
BAR 29.0 HG	250	70.0	72.4	74.5	76.9	78.8	79.5	82.0	83.1	84.9	86.6	87.6	89.1	91.4	94.4	134.2	
(97769 N/HZ)	400	76.5	77.7	79.1	79.4	78.0	78.6	80.1	82.1	83.3	84.6	84.6	83.3	82.9	81.4	80.6	
TANS 80 DEG F	500	76.0	77.7	76.1	76.8	76.4	76.2	76.1	77.8	76.7	80.9	82.3	85.5	85.5	83.7	82.2	
(294 DEG K)	600	73.5	77.1	78.2	76.9	78.8	79.2	81.5	82.5	83.6	84.6	85.6	85.6	83.7	82.2	132.3	
THET 59 DEG K	800	75.9	76.7	79.2	79.0	80.5	80.6	79.6	80.4	82.1	83.6	83.4	83.1	82.9	81.4	80.6	
(288 DEG K)	1000	75.1	77.6	78.2	78.4	77.9	78.0	77.9	79.8	81.2	83.2	84.7	84.9	83.0	81.9	81.0	
HACT 9.93 G/M3	1250	74.7	76.3	77.9	78.1	77.6	77.7	76.9	78.7	80.3	82.4	84.3	85.1	83.5	80.9	79.2	
(.00993 KG/M3)	1600	75.7	76.4	78.3	78.0	77.6	78.0	76.9	78.8	80.9	82.9	84.9	85.3	83.5	80.9	79.1	
NFA 5992 RPM	2000	74.5	76.0	77.7	77.0	76.4	76.4	76.0	78.4	80.2	81.8	83.4	84.3	82.2	79.0	77.6	
(.625 RAD/SEC)	2500	81.7	91.7	89.1	88.8	89.6	85.2	84.5	82.9	83.1	85.1	85.4	90.7	85.4	88.2	84.8	
NFK 5939 RPM	3150	72.2	82.9	81.5	83.4	81.0	79.9	79.7	79.5	80.2	82.2	84.9	87.3	81.1	82.2	79.0	
(.625 RAD/SEC)	4000	70.6	79.9	81.6	80.1	79.6	79.3	77.6	79.9	82.5	84.8	86.7	87.1	83.1	79.7	133.1	
NFD 7488 RPM	5000	79.4	85.7	87.7	86.8	84.5	84.0	81.1	82.4	84.3	86.5	88.9	90.3	85.9	85.1	83.0	
(.784 RAD/SEC)	6000	76.1	83.0	83.7	82.9	82.0	80.3	80.3	81.2	84.6	86.6	87.8	89.4	84.7	82.8	80.0	
NO. BLADES 26	8000	75.2	83.4	85.1	84.3	83.0	82.5	80.1	81.1	81.8	84.8	86.3	87.9	83.2	80.0	135.0	
	10000	72.6	81.3	83.8	83.5	81.6	81.2	78.5	79.1	81.0	82.2	84.3	85.0	81.3	80.6	77.8	
	12500	71.2	78.0	81.4	79.9	79.2	77.9	75.2	75.5	76.0	77.1	80.8	80.5	77.7	77.9	74.2	
	16000	66.6	73.5	78.2	75.8	75.4	74.6	71.1	70.9	73.4	74.4	76.8	75.5	73.8	73.4	70.3	
	20000	66.7	69.3	74.3	72.6	71.5	72.3	67.9	67.6	70.6	70.7	72.8	70.7	69.6	69.3	67.5	
OVERALL MEASURED	91.0	95.9	97.0	96.3	95.9	94.7	94.9	93.8	94.7	96.4	97.9	99.9	101.3	99.6	98.4	98.0	
OVERALL CALCULATED	89.3	95.3	95.5	94.9	94.6	94.5	93.3	92.4	93.4	94.9	96.4	98.3	101.3	97.9	98.4	147.2	
PWDB	102.7	110.0	109.3	108.8	108.9	106.8	106.0	106.1	107.6	107.6	110.4	111.9	113.0	110.8	110.7	109.4	

TABLE A7

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 90.7%N<sub>fc</sub> ; NOMINAL NOZZLE ; TREATED

PAGE 1 NASAQUIETENGINE		1/2SCALEFAN		SOUND PRESSURE LEVELS PRESENTED FOR STANDARD DAY		PROC, DATE = MONTH 12 DAY 8 HR, 20.8		ANGLES FROM INLET IN DEGREES (AND RADIANS)		PXL						
MODEL	FREQ	20	30	40	50	60	70	80	90	100	110	120	130	140	150	160
RADIAL 100, FT.	50	78.1	76.9	75.4	74.2	73.1	71.8	70.5	69.3	68.1	66.9	65.7	64.5	63.3	62.1	60.9
VEHICLE (30, M)	63	74.5	73.3	72.1	70.9	69.7	68.5	67.3	66.1	64.9	63.7	62.5	61.3	60.1	58.9	57.7
CONFIG FANB	80	71.7	70.5	69.3	68.1	66.9	65.7	64.5	63.3	62.1	60.9	59.7	58.5	57.3	56.1	54.9
LOC PTO	100	74.7	73.5	72.3	71.1	69.9	68.7	67.5	66.3	65.1	63.9	62.7	61.5	60.3	59.1	57.9
DATE 10/6/70	125	73.0	71.8	70.6	69.4	68.2	67.0	65.8	64.6	63.4	62.2	61.0	59.8	58.6	57.4	56.2
RUN 17, PT	160	73.3	72.1	70.9	69.7	68.5	67.3	66.1	64.9	63.7	62.5	61.3	60.1	58.9	57.7	56.5
TIME 17, PT	200	72.4	71.2	70.0	68.8	67.6	66.4	65.2	64.0	62.8	61.6	60.4	59.2	58.0	56.8	55.6
TYPE 17, PT	250	73.8	72.6	71.4	70.2	69.0	67.8	66.6	65.4	64.2	63.0	61.8	60.6	59.4	58.2	57.0
BAR 29.0 HG	315	80.4	79.2	78.0	76.8	75.6	74.4	73.2	72.0	70.8	69.6	68.4	67.2	66.0	64.8	63.6
(97794, N/M2)	400	80.6	79.4	78.2	77.0	75.8	74.6	73.4	72.2	71.0	69.8	68.6	67.4	66.2	65.0	63.8
TANB (23, DEG F)	500	79.3	78.1	76.9	75.7	74.5	73.3	72.1	70.9	69.7	68.5	67.3	66.1	64.9	63.7	62.5
THET (23, DEG K)	650	77.9	76.7	75.5	74.3	73.1	71.9	70.7	69.5	68.3	67.1	65.9	64.7	63.5	62.3	61.1
THET (28, DEG K)	800	78.3	77.1	75.9	74.7	73.5	72.3	71.1	69.9	68.7	67.5	66.3	65.1	63.9	62.7	61.5
HACT 9.50 GM/M3	1000	78.3	77.1	75.9	74.7	73.5	72.3	71.1	69.9	68.7	67.5	66.3	65.1	63.9	62.7	61.5
HACT 9.50 GM/M3	1250	78.4	77.2	76.0	74.8	73.6	72.4	71.2	70.0	68.8	67.6	66.4	65.2	64.0	62.8	61.6
(.00950 KG/M3)	1500	78.8	77.6	76.4	75.2	74.0	72.8	71.6	70.4	69.2	68.0	66.8	65.6	64.4	63.2	62.0
NFA 6850, RPH	2000	78.1	76.9	75.7	74.5	73.3	72.1	70.9	69.7	68.5	67.3	66.1	64.9	63.7	62.5	61.3
(.717, RAD/SEC)	2500	76.9	75.7	74.5	73.3	72.1	70.9	69.7	68.5	67.3	66.1	64.9	63.7	62.5	61.3	60.1
NFK 679, RPH	3150	84.6	83.4	82.2	81.0	79.8	78.6	77.4	76.2	75.0	73.8	72.6	71.4	70.2	69.0	67.8
(.711, RAD/SEC)	4000	74.3	73.1	71.9	70.7	69.5	68.3	67.1	65.9	64.7	63.5	62.3	61.1	59.9	58.7	57.5
NFD 7436, RPH	5000	77.5	76.3	75.1	73.9	72.7	71.5	70.3	69.1	67.9	66.7	65.5	64.3	63.1	61.9	60.7
(.784, RAD/SEC)	6000	82.5	81.3	80.1	78.9	77.7	76.5	75.3	74.1	72.9	71.7	70.5	69.3	68.1	66.9	65.7
NOI BLADES 26	8000	74.7	73.5	72.3	71.1	69.9	68.7	67.5	66.3	65.1	63.9	62.7	61.5	60.3	59.1	57.9
10000		73.1	71.9	70.7	69.5	68.3	67.1	65.9	64.7	63.5	62.3	61.1	59.9	58.7	57.5	56.3
12000		71.1	69.9	68.7	67.5	66.3	65.1	63.9	62.7	61.5	60.3	59.1	57.9	56.7	55.5	54.3
16000		66.3	65.1	63.9	62.7	61.5	60.3	59.1	57.9	56.7	55.5	54.3	53.1	51.9	50.7	49.5
20000		66.7	65.5	64.3	63.1	61.9	60.7	59.5	58.3	57.1	55.9	54.7	53.5	52.3	51.1	49.9
OVERALL MEASURED		93.7	92.5	91.3	90.1	88.9	87.7	86.5	85.3	84.1	82.9	81.7	80.5	79.3	78.1	76.9
OVERALL CALCULATED		92.3	91.1	89.9	88.7	87.5	86.3	85.1	83.9	82.7	81.5	80.3	79.1	77.9	76.7	75.5
PND8		106.1	104.9	103.7	102.5	101.3	100.1	98.9	97.7	96.5	95.3	94.1	92.9	91.7	90.5	89.3

TABLE A8



QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 58.2%N<sub>fc</sub> ; LARGE NOZZLE ; UNTREATED

PAGE 1		NASA QUIET ENGINE		1/2 SCALE FAN		PRESSURE LEVELS PRESENTED FOR STANDARD DAY		PROC. DATE - MONTH 10 DAY 17 HR. 18.8		- ANGLES FROM INLET IN DEGREES (AND RADIAN)		PWL			
MODEL SOUND		20. 30. 40. 50. 60. 70. 80. 90. 100. 110. 120. 130. 140. 150. 160.													
FREQ. (0.35)(0.52)(0.70)(0.87)(1.05)(1.22)(1.40)(1.57)(1.75)(1.92)(2.09)(2.27)(2.44)(2.62)(2.79)( )															
RADIAL 100, FT.	50	71.8	70.3	68.8	70.6	68.9	68.1	69.7	70.5	69.4	70.3	70.8	72.8	74.1	120.3
VEHICLE (30, M)	63	70.2	66.8	67.2	77.0	67.1	67.0	67.5	75.6	68.7	69.7	70.8	75.7	74.1	121.8
LOC 80	67.6	66.0	66.3	67.2	67.0	67.3	67.8	67.8	69.0	69.5	71.0	71.3	71.9	73.3	119.1
CONFIG FAN B	100	70.3	66.4	70.0	68.0	68.5	67.4	66.9	67.8	68.5	69.6	70.9	71.2	71.8	119.0
LOC 125	65.9	65.1	66.1	65.4	66.0	65.9	66.2	67.3	68.2	69.0	69.8	71.1	70.1	70.7	119.6
DATE 8/26/70	100	65.5	64.6	65.1	66.5	65.7	64.6	65.4	67.7	66.2	67.7	67.1	68.2	69.0	116.7
RUN 4. P1. 40	200	64.9	63.9	62.8	69.1	62.2	63.6	62.6	69.1	64.2	67.4	66.8	70.6	70.7	117.0
TAPE 19590	250	64.7	64.5	63.9	65.1	64.2	65.3	66.7	67.5	68.2	70.2	71.1	72.3	73.2	119.3
BAR 28.8 HG	300	65.9	66.7	67.6	69.1	68.4	68.9	69.1	71.2	72.0	73.8	74.5	75.0	75.6	122.2
(97152, N/M2)	400	67.0	69.2	71.4	70.2	70.6	69.5	70.6	72.0	73.8	74.6	75.3	75.0	74.4	122.0
TAMB 86. DEG F	500	68.6	70.5	70.1	68.8	68.4	69.0	68.4	69.3	70.9	71.7	72.8	72.4	71.0	120.6
(303, DEG K)	600	66.4	68.0	68.8	70.2	68.5	68.5	67.1	68.0	69.5	71.9	72.3	73.5	71.8	120.6
TWET 77. DEG K	800	67.8	69.7	69.2	68.2	70.7	67.4	68.4	69.7	73.0	73.1	74.5	75.2	72.9	122.0
(298, DEG K)	1000	69.6	69.0	71.7	69.2	70.1	68.4	68.4	68.8	70.8	73.0	73.6	76.2	73.9	122.0
HACT20.36 GM/MS	1250	67.1	69.7	71.6	70.4	69.8	68.5	68.5	69.4	71.0	72.8	74.7	75.6	76.2	122.2
(1.02038 KG/MS)	1600	70.1	75.0	75.0	73.1	72.5	72.0	70.8	70.8	73.6	76.1	77.8	78.6	73.9	125.2
NFA 4470. RPM	2000	79.4	86.9	86.7	83.8	84.1	83.5	81.5	82.1	84.3	86.3	87.0	86.4	85.9	135.5
(468, RAD/SEC)	2500	68.1	74.0	75.0	73.6	72.3	71.4	72.4	73.0	75.3	75.7	79.1	78.3	76.8	125.9
NFK 4356. RPM	3150	71.1	75.1	76.1	77.7	76.8	75.5	76.4	77.6	80.7	79.7	82.9	83.3	80.6	130.2
(456, RAD/SEC)	4000	75.3	84.5	85.1	84.4	83.4	82.1	80.7	82.4	84.5	86.4	86.7	89.8	83.4	136.3
NFD 7488. RPM	5000	70.2	78.7	80.9	78.1	77.4	76.7	74.8	77.2	79.4	82.1	82.2	84.5	83.8	131.4
(784, RAD/SEC)	6300	70.8	80.3	82.6	79.7	79.0	78.3	76.7	78.1	80.3	82.0	84.7	86.3	84.5	133.2
NO. BLADES 26	8000	70.0	78.2	80.3	79.3	78.5	76.8	74.5	76.9	79.9	81.0	82.6	84.9	83.9	132.4
	10000	67.0	76.1	79.3	77.1	76.0	75.0	72.8	74.3	78.6	80.6	82.3	80.8	75.8	130.9
	12500	64.2	72.9	75.1	73.8	73.2	71.5	69.1	70.1	72.4	74.5	76.9	77.5	75.8	128.1
	16000	60.1	68.2	71.6	68.8	68.8	67.8	65.0	65.8	68.7	72.6	73.1	71.8	67.9	125.8
	20000	57.5	63.4	66.9	65.5	64.5	63.3	60.8	63.1	63.6	67.7	67.0	63.4	63.4	123.7
OVERALL MEASURED	84.8	91.1	91.9	93.4	91.7	91.2	88.9	90.3	92.4	95.4	97.0	95.7	92.1	90.6	
OVERALL CALCULATED	98.1	104.5	105.4	104.5	103.7	102.6	101.5	103.2	105.1	106.8	107.7	109.8	103.5	104.6	
PNDP															

TABLE A9

100' (30.5M) ARC ; 71.8%N<sub>fc</sub> ; LARGE NOZZLE ; UNTREATED

OVERALL

85

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 78.1%N<sub>fc</sub> ; LARGE NOZZLE ; UNTREATED

PAGE 1 NASA QUIET ENGINE		1/2 SCALE FAN		PROC. DATE - MONTH 10 DAY 16 HR, 5.8															
MODEL SOUND PRESSURE LEVELS		ANGLES FROM INLET IN DEGREES (AND RADIAN)																	
		20	30	40	50	60	70	80	90	100	110	120	130	140	150	160			
FREQ.	(0.55) (0.52) (0.70) (0.87) (1.05) (1.22) (1.40) (1.57) (1.75) (1.92) (2.09) (2.26) (2.44) (2.62) (2.79) (2.97) (3.14)	50	53	56	59	62	65	68	71	74	77	80	83	86	89	92			
RADIAL 100, FT.	50	74.8	75.2	74.1	75.3	74.4	75.1	74.6	75.7	76.6	77.1	78.0	78.5	79.3	81.7	85.0			
VEHICLE (30, M)	63	72.1	72.6	73.2	74.1	74.3	74.7	75.0	75.8	76.8	77.1	78.1	79.2	79.8	82.7	85.3			
CONFIG FAN B	80	70.4	71.3	71.9	73.3	72.4	73.1	74.6	75.4	76.3	77.6	78.2	79.0	81.4	83.6				
LOC PRG	100	81.9	76.7	78.5	79.7	79.9	80.7	79.4	80.6	78.3	79.2	82.7	83.4	82.5	82.6				
DATE 8/20/70	125	74.6	72.5	73.9	74.4	74.3	74.0	74.2	74.5	74.9	76.3	77.8	79.7	78.7	79.8				
RUN 4, PT. 49	160	71.1	71.0	71.2	71.4	71.3	70.6	71.9	72.3	72.8	74.8	75.7	76.3	77.6	79.4				
TAPE T9033	200	75.6	77.3	75.0	73.6	72.5	73.3	73.0	74.6	75.0	77.0	80.4	80.0	83.4	85.3				
BAR 28.7 HG	250	68.8	70.9	72.6	73.8	73.2	75.5	77.2	78.3	79.3	81.3	82.8	84.2	85.3	86.6				
(970341 N/M2)	315	73.3	74.4	76.3	77.6	78.5	79.7	79.7	81.6	82.8	84.7	85.8	87.3	87.6	87.6				
TAN3 85 DEG F	400	74.8	76.4	78.1	78.3	77.7	79.1	79.4	80.1	81.6	82.9	83.4	83.9	83.7	83.1				
TUET 75 DEG K	500	75.0	76.6	77.1	76.0	75.4	74.8	75.2	76.8	77.9	79.8	79.8	81.3	81.2	81.5				
(333.3 DEG K)	630	73.1	76.0	77.0	77.9	77.4	77.4	77.6	79.7	81.9	82.8	83.9	84.0	83.7	82.3				
(297.168 G/M3)	800	74.5	77.6	79.9	79.0	77.0	76.0	77.3	78.4	80.0	82.3	83.3	83.3	84.6	82.2				
NFA 5991 RPM	1000	72.3	75.8	78.4	75.9	75.3	75.5	75.5	76.1	77.4	78.9	81.8	83.1	80.3	75.7				
(.01888 KG/M3)	1250	73.9	78.7	80.5	78.1	78.0	77.4	77.0	77.6	78.6	81.0	82.5	84.3	80.9	79.7				
NFK 5846 RPM	1500	72.3	79.0	80.2	79.1	77.7	77.5	77.0	78.1	78.6	81.5	82.6	84.1	79.9	78.3				
(.6271 RAD/SEC)	2000	84.7	91.3	92.8	91.9	91.3	90.5	92.3	93.3	91.4	92.8	96.1	96.0	91.1	89.1				
(.632 RAD/SEC)	3150	75.1	79.7	81.0	81.9	81.4	81.6	83.6	84.3	86.3	85.5	89.1	89.4	85.4	82.7				
(.632 RAD/SEC)	4000	72.2	81.9	82.5	82.1	82.0	82.6	83.3	85.4	85.0	88.5	88.8	90.4	85.4	82.4				
(.784 RAD/SEC)	5000	79.8	89.3	91.9	89.1	89.2	89.1	89.3	89.3	89.3	93.1	93.8	93.3	90.2	86.0				
(.784 RAD/SEC)	6300	74.0	82.6	84.2	82.0	82.0	82.0	83.5	86.0	87.0	91.9	91.9	92.1	85.8	83.5				
NO1 BLADES 26	8000	76.6	84.9	86.8	85.3	85.6	84.2	84.3	86.8	87.7	90.2	91.7	92.8	89.2	84.9				
OVERALL MEASURED	10000	72.2	81.6	84.5	81.8	81.5	80.9	81.7	84.0	84.9	87.3	89.1	90.6	94.7	82.2				
OVERALL CALCULATED	12500	68.5	78.5	80.1	79.3	78.7	77.6	78.2	80.2	81.0	84.2	85.8	85.6	77.9	78.1				
	16000	64.9	74.7	77.1	75.2	74.9	74.2	74.3	76.7	77.1	80.4	83.1	83.1	77.9	75.1				
	20000	62.5	70.7	72.9	71.1	70.8	69.9	69.7	72.2	72.4	77.1	79.2	79.4	74.2	71.0				
		91.8	97.5	99.4	97.9	97.4	97.1	98.3	99.4	101.5	103.3	104.4	100.3	99.3					
		95.8	97.7	96.2	95.8	95.3	95.3	96.2	96.8	97.8	99.9	101.8	102.8	98.8	97.9				
		104.3	110.1	111.7	110.6	110.2	109.8	110.8	110.6	111.7	113.5	115.8	116.5	112.3	110.8				

TABLE A11





QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 64.9%N<sub>FC</sub> ; LARGE NOZZLE ; TREATED

PAGE 1 NASARQUIETENGINE		1/2SCALEFAN		LEVELS PRESENTED FOR STANDARD DAY		PROC. DATE - MONTH 10 DAY 31 HR. 16.4		ANGLES FROM INLET IN DEGREES (AND RADIAN)		PWL					
MODEL	SOUND PRESSURE	20	30	40	50	60	70	80	90	100	110	120	130	140	150
FREQ. (0.35)	(0.52)	(0.70)	(0.87)	(1.05)	(1.22)	(1.40)	(1.57)	(1.75)	(1.92)	(2.09)	(2.26)	(2.44)	(2.62)	(2.80)	(2.98)
RADIAL 100' FT.	73.1	70.2	68.2	66.2	64.2	62.2	60.2	58.2	56.2	54.2	52.2	50.2	48.2	46.2	44.2
(30. M)	66.7	63.0	60.0	57.0	54.0	51.0	48.0	45.0	42.0	39.0	36.0	33.0	30.0	27.0	24.0
VEHICLE	64.5	61.2	58.0	54.8	51.6	48.4	45.2	42.0	38.8	35.6	32.4	29.2	26.0	22.8	19.6
5FAN	75.2	71.7	68.2	64.7	61.2	57.7	54.2	50.7	47.2	43.7	40.2	36.7	33.2	29.7	26.2
CONFIG FANB	68.5	65.0	61.5	58.0	54.5	51.0	47.5	44.0	40.5	37.0	33.5	30.0	26.5	23.0	19.5
100 PTO	69.5	66.0	62.5	59.0	55.5	52.0	48.5	45.0	41.5	38.0	34.5	31.0	27.5	24.0	20.5
125 DATE	69.5	66.0	62.5	59.0	55.5	52.0	48.5	45.0	41.5	38.0	34.5	31.0	27.5	24.0	20.5
160 9/19/70	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
200 RUN 14. PT. 240.	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
250 TAPE	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
315 BAR 29.0 HG	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
400 (97780) N/M2	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
TAMS 70. DEG F	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
500 (24) DEG K	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
630 TWET 63. DEG F	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
800 (290) DEG K	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
1250 MAC12.62 GM/M3	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
1600 (.03262 KG/M3)	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
NFA 4910. RPM	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
2000 (514) RPM/SEC	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
NFK 4859. RPM	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
3150 NFD (509) RAD/SEC	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
5000 NFD 7488. RPM	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
6300 (.784) RAD/SEC	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
NO: BLADES 26	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
10000	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
12500	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
16000	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
20000	63.5	60.0	56.5	53.0	49.5	46.0	42.5	39.0	35.5	32.0	28.5	25.0	21.5	18.0	14.5
OVERALL MEASURED	86.1	83.6	81.1	78.6	76.1	73.6	71.1	68.6	66.1	63.6	61.1	58.6	56.1	53.6	51.1
OVERALL CALCULATED	84.8	82.3	79.8	77.3	74.8	72.3	69.8	67.3	64.8	62.3	59.8	57.3	54.8	52.3	49.8
PND5	97.6	95.1	92.6	90.1	87.6	85.1	82.6	80.1	77.6	75.1	72.6	70.1	67.6	65.1	62.6

TABLE A14

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 79.5%N<sub>fc</sub> ; LARGE NOZZLE ; TREATED

PAGE 1 NASQUITENGINE		1/2 SCALE FAN		SOUND PRESSURE LEVELS PRESENTED FOR STANDARD DAY		PROG. DATE -- MONTH 10 DAY 31 HR. 16.4		PR - ANGLES FROM INLET IN DEGREES (AND RADIAN)		PWL	
MODEL	FREQ.	250	300	350	400	450	500	550	600	650	700
RADIAL 100' FT.	50	76.2	74.0	73.8	73.6	73.5	73.4	73.3	73.2	73.1	73.0
VEHICLE (38. M)	63	70.5	74.4	73.0	72.9	73.5	73.6	73.7	73.8	73.9	74.0
CONFIG FAN	80	67.1	69.3	70.4	71.2	71.9	72.6	73.3	74.0	74.7	75.4
LOC PTO	100	79.2	76.3	78.1	78.3	78.4	78.5	78.6	78.7	78.8	78.9
DATE 9/19/70	125	72.6	72.8	73.1	73.3	73.4	73.5	73.6	73.7	73.8	73.9
RUN 14. PT. 241	150	70.6	69.2	70.1	70.7	71.3	71.9	72.5	73.1	73.7	74.3
TAPE S1156	200	77.9	72.6	69.2	70.7	71.7	72.8	73.8	74.8	75.8	76.8
BAR 2910 M3	250	69.3	71.4	72.9	73.6	74.3	75.0	75.7	76.4	77.1	77.8
(97800) N/M2	300	75.1	76.3	77.2	77.6	78.0	78.4	78.8	79.2	79.6	80.0
TAMB 70. DEG F	350	74.9	75.4	74.7	75.4	75.7	76.1	76.5	76.9	77.3	77.7
(294) DEG F	400	72.3	73.5	74.4	75.1	75.6	76.2	76.9	77.6	78.3	79.0
TWET 63. DEG F	450	72.5	74.4	74.3	74.7	75.1	75.6	76.1	76.6	77.1	77.6
(290) DEG K	500	71.7	73.2	73.7	74.3	74.7	75.1	75.6	76.1	76.6	77.1
HAS712.62 G/H <sup>3</sup>	550	72.4	75.1	74.7	74.4	74.7	75.1	75.6	76.1	76.6	77.1
(.0122 KG/H <sup>3</sup> )	600	71.0	74.5	74.3	74.3	74.3	74.3	74.3	74.3	74.3	74.3
NFA 6015. RPM	650	79.6	87.3	91.1	91.1	91.1	91.1	91.1	91.1	91.1	91.1
(630) RAD/SEC	700	69.4	76.6	79.4	79.4	79.4	79.4	79.4	79.4	79.4	79.4
NFK 5952. RPM	750	73.4	78.4	78.1	77.9	77.9	77.9	77.9	77.9	77.9	77.9
(623) RAD/SEC	800	79.0	87.0	86.2	85.6	85.5	85.5	85.5	85.5	85.5	85.5
NFD 7488. RPM	850	71.7	79.5	80.4	80.6	80.6	80.6	80.6	80.6	80.6	80.6
(784) RAD/SEC	900	73.6	82.7	84.0	84.0	84.0	84.0	84.0	84.0	84.0	84.0
NO1 BLADES 26	950	70.4	80.4	80.9	80.9	80.9	80.9	80.9	80.9	80.9	80.9
	1000	67.6	76.7	77.7	77.7	77.7	77.7	77.7	77.7	77.7	77.7
	12500	63.5	72.3	74.3	74.3	74.3	74.3	74.3	74.3	74.3	74.3
	16000	62.8	69.1	71.1	71.1	71.1	71.1	71.1	71.1	71.1	71.1
OVERALL MEASURED	20000	88.8	94.8	96.3	96.3	96.3	96.3	96.3	96.3	96.3	96.3
OVERALL CALCULATED	80.4	93.1	94.7	94.7	94.7	94.7	94.7	94.7	94.7	94.7	94.7
PND8	101.1	106.9	109.1	109.1	109.1	109.1	109.1	109.1	109.1	109.1	109.1

TABLE A15

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 90.5%N<sub>fc</sub> ; LARGE NOZZLE ; TREATED

PAGE 1	NASA QUIET FAN	MODEL	SOUND PRESSURE LEVELS PRESENTED FOR STANDARD DAY	PROC. DATE - MONTH 10 DAY 15 HR, 11.4	ANGLES FROM INLET IN DEGREES (AND RADIANS)	PWL
RADIAL 100, FT.			20, 30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150			
(30, M)						
VEHICLE	50	78.2	(0.52)(1.07)(1.05)(1.22)(1.40)(1.57)(1.75)(1.92)(2.09)(2.27)(2.44)(2.62)(			
CONFIG	63	76.2	75.0 75.1 78.1 74.0 75.7 66.4 76.9 78.5 79.5 80.1 81.3 82.9 83.3 85.1 89.6			130.6
LOC	80	71.1	73.1 73.5 74.6 74.3 74.0 69.1 77.2 79.7 80.1 81.3 82.9 83.3 85.1 89.6			131.5
PTO	100	73.3	74.8 73.6 76.1 75.3 75.2 73.1 76.5 77.1 79.5 80.1 81.3 82.9 83.3 85.1 89.6			130.4
DATE	125	74.4	75.3 75.5 75.3 75.2 73.1 76.5 77.1 79.5 80.1 81.3 82.9 83.3 85.1 89.6			129.4
LOC	160	72.6	72.4 72.7 73.4 73.2 70.3 74.0 74.1 77.2 78.9 80.4 82.3 84.8 85.1 89.6			127.4
TAPE	200	72.2	73.3 71.7 73.4 73.2 75.2 77.2 78.7 80.8 83.1 85.2 87.8 90.0 91.4 92.8			131.9
BAR	250	74.1	76.2 76.6 78.3 78.0 80.0 80.5 81.9 83.6 85.2 88.0 89.5 91.4 92.8			135.8
	315	78.5	79.6 80.8 81.2 80.7 82.4 82.7 84.6 86.6 88.0 90.4 91.5 92.8 93.5			137.8
	400	78.8	80.2 80.9 79.5 80.0 81.4 81.7 83.2 85.3 86.4 87.9 88.2 88.6 88.6			135.1
	500	78.8	81.0 80.1 77.8 78.1 80.2 78.5 78.5 80.4 82.1 84.1 85.3 86.4 86.1			132.2
	630	75.6	77.7 77.7 77.6 78.5 81.5 80.6 82.4 85.0 85.6 87.4 87.4 88.5 86.8			134.4
	800	76.9	79.3 79.4 79.1 80.1 82.3 81.1 82.2 84.0 84.7 85.9 85.0 85.7 84.9			133.4
	1000	76.5	78.8 79.6 79.6 79.5 81.6 80.4 81.9 83.9 85.6 87.4 86.6 86.3 85.1			133.2
	1250	75.9	79.4 80.8 78.9 80.7 82.0 79.5 80.9 82.6 83.5 86.1 85.7 85.8 84.6			133.9
	1600	78.6	81.6 81.6 82.0 82.7 83.4 80.5 81.2 83.4 84.4 85.7 85.7 84.3			133.1
	2000	77.1	81.6 80.8 80.4 82.0 83.0 78.9 80.1 82.4 83.7 84.1 85.7 84.5			133.1
	2500	76.9	83.1 85.4 83.8 82.2 83.3 81.0 79.5 81.3 82.3 84.9 85.6 83.3 84.6			133.8
	3150	84.5	91.6 94.7 93.3 90.4 91.4 89.6 97.0 88.2 87.7 92.7 91.9 89.9 93.8			141.9
	4000	77.6	84.8 85.6 85.8 84.5 86.7 83.3 84.1 86.3 87.1 89.1 89.0 85.7 86.3			137.3
	5000	78.1	84.7 84.9 84.2 85.4 86.0 82.2 85.0 86.3 88.3 90.0 90.1 86.6 85.0			137.7
	6300	78.3	86.8 86.6 86.5 86.7 86.7 85.6 85.0 88.3 90.9 93.0 92.5 89.2 86.8			140.5
	8000	74.4	82.8 85.1 84.3 83.5 85.3 83.0 84.1 86.8 88.4 89.9 90.5 85.6 84.9			138.3
	10000	72.8	82.4 83.5 82.4 82.5 84.2 81.0 82.3 84.8 86.8 88.4 89.9 85.4 83.1			135.9
	12500	69.5	78.5 80.8 79.3 79.3 80.2 77.7 79.6 82.1 84.2 85.4 85.7 81.5 80.0			133.8
	16000	65.1	74.5 76.8 74.1 74.8 76.2 73.6 74.8 77.0 79.3 81.4 81.6 78.5 75.8			133.1
	20000	62.9	70.5 72.7 70.3 70.5 72.0 69.4 71.3 73.3 75.3 77.0 78.5 77.7 73.7			149.9
	OVERALL MEASURED	92.4	98.0 99.6 98.7 97.7 99.0 97.1 97.3 99.4 100.9 103.0 103.2 102.5 103.3			
	OVERALL CALCULATED	91.2	96.4 98.2 97.2 96.2 97.4 95.6 96.0 98.0 99.4 101.6 101.8 101.2 102.2			
	PND8	105.6	111.5 113.5 112.5 111.0 112.1 110.3 109.6 111.3 112.4 115.1 115.0 113.6 115.3			

TABLE A16



QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 59.0%N<sub>fc</sub> ; SMALL NOZZLE ; UNTREATED

PAGE 1	NASA QUIET ENGINE	1/2 SCALE FAN	PRESSURE LEVELS PRESENTED FOR STANDARD DAY	PMUC	DATE	FROM INLET IN DEGREES (AND RADIAN)	PHL																													
MODEL	SOUND	20	30	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360
RADIAL 100 FT	50	60	70	80	90	100	110	120	130	140	150	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400
VEHICLE (301 M)	60	70	80	90	100	110	120	130	140	150	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	
CONFIG 13 FAN	100	110	120	130	140	150	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450
LOC 821/70	120	130	140	150	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470
DATE 8/21/70	140	150	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490
RUN 9, PT, 61	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510
TAPE S1105	180	190	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530
BAK 2818 HG	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	
(972021 NMH2)	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	
IAMB (2951 DEG K)	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	
INLET 621 DEG K	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	
MAG13106 GMH3	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	610	620	
NFA14501 RPN	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	610	620	630	640	
NFK (4021 RAD/SEC)	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	610	620	630	640	650	660	
NFD (4621 RAD/SEC)	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	610	620	630	640	650	660	670	680	
NFD (74881 RPN)	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	610	620	630	640	650	660	670	680	690	700	
NFD (78811 RAD/SEC)	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	610	620	630	640	650	660	670	680	690	700	710	720	
NOI BLADES	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	610	620	630	640	650	660	670	680	690	700	710	720	730	740	
OVERALL MEASUREMENTS	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	610	620	630	640	650	660	670	680	690	700	710	720	730	740	750	760	
OVERALL CALCULATIONS	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	610	620	630	640	650	660	670	680	690	700	710	720	730	740	750	760	770	780	

TABLE A17



100' (30.5M) ARC ; 79.0%N<sub>fc</sub> ; SMALL NOZZLE ; UNTREATED

[illegible]

TABLE A19

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 90.6%N<sub>FC</sub> ; SMALL NOZZLE ; UNTREATED

PAGE 1 NASA QUIET ENGINE		1/2 SCALE FAN		PROC. DATE - MONTH 8 DAY 31 HR. 6.3		ANGLES FROM INLET IN DEGREES (AND RADIANS)		PKL
MODEL	SOUND PRESSURE LEVELS PRESENTED FOR STANDARD DAY	20	30	40	50	60	70	
FREQ. (0.35)(0.52)(0.70)(0.87)(1.05)(1.22)(1.40)(1.57)(1.75)(1.92)(2.09)(2.27)(2.44)(2.62)(2.79)(3.00)	20	30	40	50	60	70	80	90
RADIAL 100, FT. (30, M)	50	77.2	76.6	74.6	76.8	76.1	76.9	77.7
VEHICLE	63	74.3	74.6	75.3	80.1	76.1	77.4	78.3
CONFIG .5 FAN	80	72.6	73.8	74.3	75.3	75.1	76.2	77.3
LOC PPG FAN B	100	76.1	75.6	74.6	77.7	77.6	78.4	79.3
DATE 8/21/70	125	78.1	76.5	76.5	78.5	78.1	79.6	80.0
RUN 5, PI. 76	160	74.8	73.9	73.8	73.9	74.8	74.4	75.7
TAPE	200	74.4	74.5	73.4	75.1	75.1	76.3	75.7
BAR 28.8 H3 S11.08	250	76.7	77.2	78.6	81.0	80.2	81.2	83.0
(97250, N/M2)	315	80.7	81.2	83.9	83.8	83.8	84.1	85.3
TAB 70, DEG F	400	81.6	82.0	83.6	82.6	82.6	82.4	83.9
(284, DEG K)	500	81.2	81.4	80.9	81.7	81.9	82.2	83.1
THET 63, DEG F	600	79.6	80.4	80.6	80.3	80.1	81.2	81.8
(299, DEG K)	1000	79.2	81.1	82.0	81.9	81.9	82.4	82.7
HACT12.63 CV/M3	1250	78.4	80.6	83.4	82.2	82.5	82.9	83.0
(.01263 KG/M3)	1600	80.0	83.4	84.3	83.8	84.0	84.0	84.4
NFA 6860, RPM	2000	78.9	83.8	83.4	83.2	83.6	84.1	85.1
(.718, RAD/SEC)	2500	78.0	84.1	85.4	85.1	85.3	84.5	85.3
NFK 6250, RPM	3150	84.2	90.9	94.6	93.3	94.6	94.3	90.7
(.711, RAD/SEC)	4000	79.7	86.4	87.7	85.3	86.2	86.5	86.8
NFD 7488, RPM	5000	80.6	87.7	88.4	86.9	86.6	86.8	88.2
(.784, RAD/SEC)	6000	82.1	91.9	94.7	90.1	90.6	90.4	90.3
NO, BLADES 26	8000	77.4	86.1	88.6	89.0	86.7	86.3	85.4
	10000	76.6	86.3	87.9	87.0	86.1	84.9	85.8
	12500	71.4	82.5	83.7	83.6	82.6	81.9	82.0
	15000	69.0	80.1	80.9	80.4	79.5	78.6	78.5
	20000	65.9	75.7	76.9	76.2	75.1	74.3	73.7
OVERALL MEASURED	94.5	99.9	101.4	101.2	100.8	99.7	98.6	98.2
OVERALL CALCULATED	93.1	98.4	99.9	99.3	98.2	97.2	96.3	95.8
P: DB	106.8	112.3	114.6	114.9	114.3	112.6	112.7	112.6

TABLE A20

100' (30.5M) ARC ; 58.6%N<sub>fc</sub> ; SMALL NOZZLE ; TREATEDTABLE A21

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 72.3%N<sub>fc</sub> ; SMALL NOZZLE ; TREATED

PAGE 1 NASA QUIET ENGINE 1/2 SCALE FAN																
MODEL SOUND PRESSURE LEVELS PRESENTED FOR STANDARD DAY - ANGLES FROM INLET IN DEGREES (AND RADIAN),																
PRIC. DATE - MONTH 10 DAY 28 HR. 14.6																
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TABLE A22

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 78.6%N<sub>fc</sub> ; SMALL NOZZLE ; TREATED

PAGE 1 NASA QUIET ENGINE 1/2 SCALE FAN										PROC. DATE - MONTH 10 DAY 28 HR, 14:6									
MODEL SOUND PRESSURE LEVELS PRESENTED FOR STANDARD DAY - ANGLES FROM INLET IN DEGREES (AND RADIAN)																			
RADIAL 100, FT.	20	30	40	50	60	70	80	90	100	110	120	130	140	150					
(30, M)	50	60	70	80	90	100	110	120	130	140	150								
VEHICLE	50	60	70	80	90	100	110	120	130	140	150								
LOC	50	60	70	80	90	100	110	120	130	140	150								
DATE	50	60	70	80	90	100	110	120	130	140	150								
PTC	50	60	70	80	90	100	110	120	130	140	150								
5/19/70	50	60	70	80	90	100	110	120	130	140	150								
13, PT, 223	50	60	70	80	90	100	110	120	130	140	150								
TAPE	50	60	70	80	90	100	110	120	130	140	150								
1156	50	60	70	80	90	100	110	120	130	140	150								
28,9 HS	50	60	70	80	90	100	110	120	130	140	150								
(977561 N/MH2)	50	60	70	80	90	100	110	120	130	140	150								
TANG 78, DEG F	50	60	70	80	90	100	110	120	130	140	150								
(299, DEG K)	50	60	70	80	90	100	110	120	130	140	150								
THET 65, DEG F	50	60	70	80	90	100	110	120	130	140	150								
(291, DEG K)	50	60	70	80	90	100	110	120	130	140	150								
HACT 11,90 G/M3	50	60	70	80	90	100	110	120	130	140	150								
(,01190 K3/M3)	50	60	70	80	90	100	110	120	130	140	150								
NFA 5920, RPM	50	60	70	80	90	100	110	120	130	140	150								
(,627, RAD/SEC)	50	60	70	80	90	100	110	120	130	140	150								
NPK 5833, RPM	50	60	70	80	90	100	110	120	130	140	150								
(,616, RAD/SEC)	50	60	70	80	90	100	110	120	130	140	150								
NFD 7488, RPM	50	60	70	80	90	100	110	120	130	140	150								
(,764, RAD/SEC)	50	60	70	80	90	100	110	120	130	140	150								
NO, BLADES 26	50	60	70	80	90	100	110	120	130	140	150								
OVERALL MEASURED	50	60	70	80	90	100	110	120	130	140	150								
OVERALL CALCULATED	50	60	70	80	90	100	110	120	130	140	150								
PND8 103.5	50	60	70	80	90	100	110	120	130	140	150								

TABLE A23

QEP SCALE MODEL FAN B  
1/3 OCTAVE DATA CORRECTED TO STANDARD DAY  
100' (30.5M) ARC ; 89.8%N<sub>fc</sub> ; SMALL NOZZLE ; TREATED

PAGE 1 NASA QUIET FAN															
MODEL		PROC. DATE - MONTH 10 DAY 15 HR. 11.4													
		FROM INLET IN DEGREES (AND RADIAN)													

TABLE A24



## X. NOMENCLATURE

A	Nozzle Area
B&K	B&K Instruments, Inc. - Bruel & Kjaer Precision Instruments
D.I.	Directivity Index, the sound pressure level at a particular position and frequency minus the spaced average sound pressure level at that frequency.
$f_1$	Fan blade passing frequency fundamental
$f_2$	Fan blade passing frequency second harmonic
$F_n$	Net engine thrust
$M_o$	Aircraft Mach Number
$N/\sqrt{\theta}$	Fan rotational speed, corrected to standard day
Nom.	Nominal
OAPWL	Overall sound power level calculated by summation of power level spectra from 50 Hz to 20K Hz.
OASPL	Overall sound pressure level calculated by summation of sound pressure levels at each 1/3 octave from 50 Hz to 20K Hz.
O.B.	Octave band
O.G.V.	Outlet guide vane
$P_{T23}/P_{T2}$	Ratio of fan bypass exit total pressure to fan inlet total pressure
PNL	Preceived noise level; a calculated, annoyance weighted sound level
PWL	Sound power level, Re $10^{-13}$ watts
QEP	Quiet Engine Program
RMS	Root mean square
SL	Sideline
SLS	Sea level static
SPL	Sound pressure level, Re $.0002 \text{ dynes/cm}^2$
$V_{\text{plane}}$	Aircraft velocity
$\frac{W_{\text{bypass}} \sqrt{\theta}}{\delta}$	Bypass air flow, corrected to standard day
dB	Decibel
Hz	Hertz (cycles per second)
ips	Inches per second
PNdB	Preceived noise decibel

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